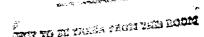
NASA Technical Paper 1747

Assessment of Ground Effects on the Propagation of Aircraft Noise:

The T-38A Flight Experiment



William L. Willshire, Jr.

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Assessment of Ground Effects on the Propagation of Aircraft Noise: The T-38A Flight Experiment

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Scientific and Technical Information Branch

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SUMMARY

A flight experiment was conducted to investigate air-to-ground propagation of sound at grazing angles of incidence. A turbojet-powered airplane was flown at low altitudes over two microphone arrays. The first array consisted of 8 microphones positioned along a 2500-m concrete runway. The second array consisted of 12 microphones positioned over grass parallel to the runway. Twenty-eight flights were made at altitudes ranging from 10 to 160 m. The acoustic data have been reduced to 1/3-octave band spectra and time correlated with the tracking and weather information. Acoustic, tracking, and weather information are presented in the appendices in a form which will allow independent analysis of the data.

The dependence of ground effects on frequency, incidence angle, and slant range has been determined using two analysis methods. In the first, referred to as the near/far comparison method, acoustic data from a microphone close to the flight track are compared with data from down-range microphones positioned over grass. The second method used is a direct comparison between two microphones equidistant from the flight track but positioned over the two different surfaces. In both methods, source directivity angle was the criterion by which portions of the microphone signals were compared.

The results of the two analysis methods were in general agreement. The ground effects were largest in the frequency range of 200 to 400 Hz and were found to be dependent on incidence angle and on slant range. Ground effects measured for angles of incidence greater than $10^{\rm O}$ to $15^{\rm O}$ were near zero. Measured attenuation increased with increasing slant range for slant ranges less than 750 m. Theoretical predictions were found to be in good agreement with the major details of the measured results.

INTRODUCTION

The levels of noise received on the ground from an aircraft are strongly influenced by the ground as a reflecting-absorbing boundary. When the aircraft is close to the ground during takeoff and landing, noise is emitted at grazing angles to a sideline observer. The signal received at the sideline is different, by as much as 20 dB for certain frequencies, from what would be expected considering only the effects of spherical spreading and atmospheric absorption. The difference between measured and expected sideline noise levels is referred to as lateral attenuation.

Lateral attenuation is not due solely to ground effects. At low elevation angles, shielding effects of the aircraft on the emitted noise may substantially alter the received signal. Lateral attenuation should be separated into shielding effects and ground effects because of their differing physical origins. Shielding effects are aircraft dependent, while ground effects are functions of

ground properties such as porosity and roughness. A basic understanding of the effects contributing to lateral attenuation is required for accurate prediction of aircraft noise.

A procedure for predicting propagation effects on aircraft noise was given by Putnam (ref. 1) in 1975. For predicting ground attenuation, Putnam recommended the empirical curves developed by Franken and Bishop (ref. 2) for ground-to-ground propagation in conjunction with civil noise-exposure-forecast (NEF) transition curves (given in ref. 3) for air-to-ground propagation. The NEF curve, which illustrates the dependence of ground attenuation on aircraft elevation angle, has a sharp cutoff of ground effects above about 7° elevation; whereas, other estimates have been made that ground effects persist for elevation angles up to 30°, 50°, or even 70° (ref. 1).

Pao, Wenzel, and Oncley (ref. 4) have proposed an analytically based prediction method for ground effects to replace Putnam's empirical method. Ground reflection and attenuation are included in the analytical method for ground-to-ground and air-to-ground propagation. The empirical ground-impedance formula by Delany and Bazley (ref. 5) is used in the prediction method. In agreement with Putnam's method, the analytical procedure predicts that ground attenuation of aircraft noise decreases quickly, but smoothly, with increasing elevation angles.

A widely used data set on ground-to-ground propagation over large distances was developed by Parkin and Scholes (refs. 6 and 7) in the middle 1950's. They used a small turbojet engine as a noise source and made measurements at logarithmically spaced intervals, to distances of 7 km, over a grassy terrain. Data were recorded under varying weather conditions over a period of one year at two sites in England. Zorumski (ref. 8) has found fair-to-good agreement between the prediction method of Pao, Wenzel, and Oncley and the data of Parkin and Scholes. Although data scatter is large (due to variable weather and terrain conditions), the theory and the data show that ground attenuation effects are largest in a frequency range from about 200 to 2000 Hz. The theory also correctly predicts the magnitude of the ground attenuation and the ground reflection effects.

A flight experiment was conducted by Benson, Karplus, Burkhard, Sabine, and Raelson (refs. 9 to 12) to study the influence of weather on air-to-ground propagation. The results of their study indicated that ground attenuation was a function of angle, with little attenuation measured for elevation angles greater than 140, and that the ground attenuation increased linearly with frequency from 75 to 2400 Hz. Walker has gathered data from several aircraft and developed empirical curves for the ground attenuation as a function of frequency and elevation angle (ref. 13). His curves indicate large attenuation effects (10 to 20 dB) at frequencies below 200 Hz. This is in sharp disagreement with the predictions and with the Parkin and Scholes data. Mashita and Bauer (ref. 14) have analyzed data from three aircraft and found attenuation effects in the frequency range from 200 to 2000 Hz, which roughly agree with the lowangle predictions. However, their results do not show the predicted rapid decrease of attenuation with elevation angle. Mashita and Bauer also isolated aircraft-dependent lateral attenuation effects and recommended that the curve with least lateral attenuation be used for the ground attenuation.

The purpose of this paper is to analyze a comprehensive data base, the T-38 excess-ground-attenuation-experiment data, for ground effects on air-to-ground noise propagation. The T-38 experiment is described in detail in reference 15 and was intended to complement the data of Parkin and Scholes by including the elevation angle of the acoustic source as a variable. Shallow angles are emphasized since data are needed in this regime to settle the questions of the dependence of ground attenuation on angle. A turbojet air-plane, powered by a single rear-mounted engine, is used as a noise source in order to minimize shielding effects. Ground effects are calculated from the data to determine the variation of these effects with frequency, elevation angle, and slant range. A theoretical model is chosen and used to make predictions of the ground effects to compare with the measured results. Basic data on the airplane flights, the weather, and the noise are included as appendices so that independent studies of these data may be conducted by other researchers.

SYMBOLS

a	dimensionless nonnegative number
A	complex number
co	speed of sound
f	frequency
F (τ)	function defined by equation (4)
Im(A)	imaginary part of complex number A
k	wave number
k _o	wave number of 1/3-octave bandcenter frequency
p^2	mean square pressure
p_0^2	free-field mean square pressure
r ₂	total path length of reflected wave
R	magnitude of complex reflection coefficient
W	complex error function
X,Y,Z	data reduction coordinates
z	acoustic ground impedance
α	phase of complex reflection

- β elevation angle
- Γ plane wave reflection coefficient
- Δr difference in length between reflected and direct paths
- n defined by equation (8)
- θ angle between reflected wave path and ground
- v normalized acoustic admittance of ground
- ρ_{O} ground level density
- ground flow resistance
- t defined by equation (5)

Abbreviations:

EPNL effective perceived noise level

G.m.t. Greenwich mean time

NEF noise exposure forecast

SPL sound pressure level

SR slant range

DESCRIPTION OF EXPERIMENT

Test Site

The flight program was conducted during the first week of November 1978 at the NASA Wallops Flight Center. Figure 1 is a photograph of the general experimental site. The aircraft flight track was along runway 10-28; the flight track direction was from the top left to the top right of the figure. The microphone arrays were located along runway 04-22, a 2500-m long, 50-m wide, landing research runway and in the grassy area to the left (north), between the runway and the taxiway. The radar tracking site was located to the left of the intersection of runways 04-22 and 10-28.

The grassy area may be described as covered with institutional grass which was cut every week. The width of the grassy area was 115 m for the wider portion and 70 m for the narrower portion, close to the flight track. The soil under the grass was a mixture of sand and clay and was dry because the area had received less than 1.3 cm of rain within the 30 days before the test.

Aircraft

The airplane used in the experiment is shown in figure 2. The airplane was powered by two turbojet engines with afterburners. Each engine develops 11 930 N of thrust at military power setting, 17 130 N of thrust with afterburning, and 490 N of thrust at flight idle. Listed in table I are additional engine parameters. A laser tracker was used to determine aircraft position, which was calculated in Cartesian coordinates oriented with respect to the runways as shown in figure 3, every 1/2 sec Greenwich mean time (G.m.t.).

Constraints for unambiguous tracking are: ranges between 100 m and 36 000 m; radial velocities less than 3048 m/sec; and radial acceleration less than 0.45 rad/sec. Tracking system accuracy is estimated to be ± 0.5 m.

The airplane was equipped with two laser reflector cube housings. The main reflector was located on a centerline pylon 7.2 m forward of the exhaust nozzle exit and 0.6 m below the engine centerline. A secondary reflector was located on the aft fuselage 2.2 m forward of the nozzle exit, 0.2 m above the engine centerline, and 0.7 m laterally from the centerline. Speed brakes are shown in figure 2 in the deployed position behind the main laser reflector. Exhaust nozzles are 0.4 m in diameter with 0.5-m centerline spacing. The nozzle centers are 1.4 m above the ground plane and protrude 0.6 m behind the aircraft fuselage.

In order to minimize flight speeds, the landing gear and speed brakes were deployed. During the incoming flight, the laser tracker locked onto the main reflector. However, the speed brakes and main-landing-gear doors obstructed the line of sight to the main reflector after the aircraft passed the tracking station. Hence, the aircraft was tracked during the outgoing flight by the secondary reflector. The loss of track introduced gaps in the tracking information ranging from 3 to 7 sec. In processing the flight tracks, a straight line was interpolated between the gap endpoints.

There were 28 flights (runs) in 2 days of testing. For every run, the flight path of the airplane was from west to east above the centerline of runway 10-28 at a prescribed altitude. The airplane was flying at the particular run conditions at least 800 m before and after the intersection of runways 04-22 and 10-28. The various runs and their corresponding flight conditions are listed in table II. For the majority of the flights, the number one (left) engine was at flight idle and the number two (right) engine was at a nominal power setting of 100 percent. Two runs were flown at an altitude of 18 m with the number two engine in full afterburner. Run 28 was done under ground-static conditions.

Figure 4 is an illustration of the laser track for run 26. In the figure, the three-dimensional tracking information is split into 2 two-dimensional views: an X-Y view and an X-Z view. The X-Y view includes an outline of the Wallops runways used in the test and the microphone positions, labeled 1 to 20, to be discussed in the next section. The microphone locations are along runway 04-22, and the aircraft's ground track is the dashed line along runway 10-28. Evident in the X-Z view is the straight line that has been computed to fill in a gap in the tracking information due to loss of track.

Acoustic Instrumentation

The acoustic instrumentation consisted of 20 microphone systems located in 5 mobile vans. The microphone positions are illustrated in figure 5, and their Cartesian coordinates are listed in table III (in the runway-fixed coordinate system). The components of a microphone system are illustrated in block form in figure 6.

To document the system's linearity, sensitivity, distortion, and noise floor, each acoustic instrumentation system was laboratory calibrated prior to going into the field. The results of the laboratory calibrations were used to insure that the equipment operated within the manufacturer's specifications. A piston phone was used in the field for level calibration, and a pink noise source was used for frequency response calibration. The acoustic signals recorded were time correlated with G.m.t.

Weather Instrumentation

Weather measurements were made at a number of locations along runway 04-22. Wind speed, wind direction, temperature, and relative humidity were measured with portable 1.2-m weather stations located near vans 1 and 5 (see fig. 5) in the open areas south of runway 04-22. A 10-m-high portable weather station located near van 2 measured barometric pressure in addition to the variables measured by the 1.2-m stations. The output of the 1.2-m stations was in the form of strip charts, while the output of the 10-m station was digitally encoded and recorded on the magnetic tape recorder in van 2. The output of the 10-m station could also be conveniently read in a real-time mode inside the van. Detailed descriptions of both types of weather stations may be found in reference 16.

A retrievable balloon was used to raise one weather measuring instrument package. Profiles of temperature, relative humidity, and wind speed, up to an altitude of 500 m, were measured with the balloon package. The altitude of the package was computed from pressure differences between the measured ground pressure and the pressure measured aloft. The output of the package was telemetered down to an instrument van on the ground, where it was displayed in a real-time mode and was encoded and recorded on magnetic tape. The balloon weather station is described in more detail in reference 17.

Additional weather information was obtained from three permanent weather stations located in building N-159, in building C-15, and in the triangle area. The station at N-159 has a sensor height of 10 m, the sensor height at C-15 is 4 m, and the triangle station sensors have heights of 3, 6, 9, 12, and 15 m. Each station was instrumented to measure wind speed, wind direction, and temperature. The N-159 site was also equipped for the measurement of dew point and barometric pressure. The outputs of the N-159 and C-15 sites were in the form of strip charts, while the triangle site output was in the form of computer listings.

A representative sample of the weather information obtained from the ground stations is illustrated in table IV for run 27. Weather data for each run, as

well as profiles of wind speed, temperature, and relative humidity taken through use of the instrumented balloon package, are given in appendix B.

Acoustic Data

The analog tapes of the flyover noise were reduced by 1/3-octave band analysis. The frequency range of the analysis was from 20 Hz to 10 kHz with an averaging time of 1/8 sec. The 1/8-sec averaging time was necessary because of the large angular velocity of the aircraft with respect to the microphones closest to the flight path. The 1/3-octave band analysis was initiated for each run when the incoming aircraft was approximately 800 m from the intersection of runways 04-22 and 10-28. The analysis was stopped when the amplitude of the noise received from the aircraft approached that of the background noise. Associated with each 1/3-octave spectrum is a G.m.t., an overall sound pressure level (SPL), and a dBA level.

The piston-phone calibration was used to calibrate the amplitude of the 1/3-octave band analysis system. The pink-noise calibration was used to correct for deviations from a flat frequency response of the record/playback system.

The quality of the reduced acoustic data was first checked by inspection of the overall time histories for each microphone for each run. Overall time histories for microphones 2, 4, 6, and 8 for run number 27 are illustrated in figure 7. Broadening of the shape of the airplane noise time history occurs as the distance from microphone to flight path increases with microphone number. This may be seen in figure 7. The effect of atmospheric propagation anomalies are noted by the roughness in the signals from the further microphone locations because of the longer propagation distances and the smaller signal-to-noise ratios.

Ambiguities may exist in the results of the lower frequency 1/3-octave bands because of the 1/8-sec averaging time. The 1/3-octave band analyzer used in the data reduction process passes an input signal in parallel through various, active 1/3-octave band filters and selectively samples the output of the filters. The limiting feature of this analysis for the present application is the response time of the filters. A customary manner of characterizing filter response is to compute a so-called "BT" product (bandwidth multiplied by time width of the signal); a BT product greater than 50 is considered satisfactory. For the 100-Hz 1/3-octave band at an analysis time of 1/8 sec, the BT product is 6. The reduced data at the lower frequency bands must be viewed with the limited response times of the filters in mind. However, the lower frequency results to be given later appear to be consistent with the higher frequency results.

Spectra from run 27 for microphones 2, 4, 8, and 16, at the time of their respective maximum overall sound pressure levels, are shown in figure 8. Observed in the last three spectra of figure 8 is a double hump formation which broadens (over a number of 1/3-octave bands) and deepens with increasing propagation distance.

METHODS OF ANALYSIS AND THEORY

Various methods may be used to determine ground effects. Most methods are comparative in nature in that a relative difference is determined between two microphone signals. After a methodology is chosen, the manner in which the portions of the signals to be compared are selected becomes a critical issue. Criteria which may be used to select the portions of the signals are maximum overall level, maximum level in a particular 1/3-octave band, closest point of approach, and sound emission angle, to name a few. From a trial-and-error approach, two methods to compute ground effects were found to be the most reliable and consistent. They are described in this section. Included in the discussion is the criteria used to select the portions of the signals to be compared.

Comparison of Near and Far Microphones

The method used by Parkin and Scholes (refs. 6 and 7) to calculate ground effects was a comparison in the frequency domain of near and far microphones positioned over the same terrain. In this method, a microphone close to the acoustic source is chosen as a reference microphone, and its signal is compared to the signals from the remaining microphone locations, referred to as measurement microphones. Corrections are made to the reference microphone signal for differences in spherical spreading and atmospheric absorption between the measurement and reference microphone locations. The difference between the corrected reference spectrum and the measurement spectrum is a measure of the relative difference in ground effects between the two positions. If the reference microphone signal is free of ground effects, the procedure results in a measure of the absolute ground effect at the measurement location.

In practice, the method of comparing near and far microphones must account for the directivity of the source. With a static experiment like that of Parkin and Scholes, the problem of differences in source directivity was not large. In their experiment, all of the microphones were of the same height and were placed on a radial line from the source, and the dimensions of the source were small compared to the distance to the first microphone. As an aircraft flies by a microphone, however, the emission directivity angle of the received signal is constantly changing. For flight work, the solution is to insure that the signals from the two microphones to be compared have the identical source emission angle. The problem of directivity synchronization involved in comparing two signals from different microphones in a flight experiment is a major one.

For the present study, implementation of the near/far comparison method was accomplished with the aid of a computer. A free-field source spectrum was used as the reference spectrum. This source spectrum was determined by averaging spectra from runs 17 to 24, 26, and 27 for microphone 15. These 10 runs were selected because they were taken under more ideal weather conditions. For the results to be given later, the following subset of the 10 runs was selected (the subset represents 1 run for each altitude): 17, 21, 24, 26, and 27. Microphone 15, a 10-m microphone positioned over concrete close to flight path, was selected because it had more readily predictable ground effects. The

spectra for each run to be averaged were selected from an emission angle criterion. Before averaging the 10 spectra, the effect of ground reflections were removed, as detailed below, and the spectra were corrected for atmospheric absorption and spherical spreading to a slant range of 10 m.

Because of the oblique angle between the microphone arrays and the flight track in the T-38A flight experiment, the sound emitted from the airplane at an emission angle of 122.50 (referenced to the forward inlet direction) propagated parallel to the microphone arrays. For a particular run, values were calculated for the time and position of the aircraft at which the sound emitted propagated parallel to and over the microphone array containing microphone 15 (the sound emitted at a directivity angle of 122.50, see fig. 9). These values are referred to as the emission time and position. The propagation time from this aircraft position to microphone 15 was then calculated using an average speed of sound, which was calculated using a layered model of the atmosphere incorporating measured weather parameter profiles. The reception time was defined as the sum of the emission time and the propagation time. The two 1/3-octave band spectra of the time history for microphone 15 located on either side of the reception time were averaged together to form a spectrum for the particular run. The averaging of two 1/8-sec spectra gives an effective averaging time of 1/4 sec for the resulting spectrum.

Corrections computed with the ground-effects prediction procedure (to be discussed later in this section) were applied to the spectra to remove the influence of ground reflections. The value of the input parameters necessary for the procedure were set to the same values as those used in a later section of this report for a microphone positioned over concrete. Atmospheric absorption corrections were calculated using the American National Standards Institute (ANSI) standard method for the determination of molecular absorption (ref. 18). The resulting reference spectrum is illustrated in figure 10. The solid curve is the average spectrum at 10 m with ground effects removed and is the spectrum used as the reference spectrum in the near/far comparison method.

After the reference spectrum has been determined, the near/far method is implemented by selecting a measurement microphone for a particular run and determining the measurement spectrum in a similar fashion. The reference spectrum is brought to the same slant range as the measurement spectrum by incorporating losses for spherical spreading and atmospheric absorption. The measurement spectrum is subtracted from the reference spectrum to yield a ground effects spectrum for the particular geometry (measurement microphone and run) chosen. Subtracting the measurement spectrum from the reference spectrum defines a positive sign for an attenuation and a negative sign for an amplification for the ground effects at the measurement microphone.

Comparison of Microphones Over Concrete and Grass

The second method used to analyze ground effects is a direct comparison between two microphones equally distant from the acoustic source but positioned over different surfaces. An advantage of the direct comparison method is that there is no need to use corrections for differences in spherical spreading and atmospheric absorption between the two signals to be compared. The direct

comparison method has the same source directivity problem as the previous comparative method. To solve the problem, the source emission angles of the two signals to be compared are again constrained to be equal. The difference is then taken between the signals of the two microphones in the frequency domain. The result is a spectrum which is a measure of the relative difference in ground effects between the two microphone locations.

Implementation of the direct comparison method begins with the selection of a microphone pair and a run number. For the present study, the possible microphone pairs which are equal distance from the flight path and positioned over grass and concrete, respectively, are microphones 1-13, 2-14, 3-15, 8-18, 9-19, and 11-20. The emission angle criterion of 122.5° is again used to determine a spectrum from each microphone of a pair for the chosen run. The spectrum for the microphone positioned over grass is subtracted from the spectrum for the microphone over concrete to yield a ground effects spectrum. The spectrum represents the differences in ground effects between the two locations for the two surfaces with similar geometry between the microphones and the aircraft. A positive value signifies a lower level received at the microphone over grass as compared to the microphone over concrete.

Theoretical Predictions of Ground Effects

The theoretical model chosen to make ground effects predictions is the procedure recommended by Pao, Wenzel, and Oncley (ref. 4). This prediction method was employed by Zorumski (ref. 8) to make comparisons with the Parkin and Scholes (refs. 6 and 7) ground effects data and some aircraft flight data. The formulation of the method is based on work by Chien and Soroka (ref. 19) and Thomasson (ref. 20). The predicted mean square pressure p^2 at the observer position is

$$\frac{p^2}{P_0^2} = 1 + 2R \exp(-ak \Delta r)^2 \cos (\alpha + k \Delta r) + R^2$$
 (1)

where ${p_0}^2$ is the mean square pressure without ground effect (free-field mean square pressure), R and α are the magnitude and phase of the complex reflection coefficient, a is a dimensionless nonnegative number, k is the wave number, and Δr is the difference in length between the reflected path and the direct path.

The complex reflection coefficient is defined here as

$$Re^{i\alpha} \equiv \Gamma + (1 - \Gamma) F(\tau)$$
 (2)

where Γ is the plane-wave reflection coefficient

$$\Gamma = \frac{\sin \theta - \nu}{\sin \theta + \nu} \tag{3}$$

 θ is the angle between the reflected wave path and the ground (see fig. 9), and ν is the normalized acoustic admittance of the ground. The function $F(\tau)$ is given by

$$F(\tau) = 1 - \tau W(i\tau) \sqrt{\pi}$$
 (4)

with

$$\tau = (\sin \theta + \nu) \sqrt{\frac{kr_2}{2i}}$$
 (5)

where r_2 is the total path length of the reflected wave, and W is the complex error function defined by

$$W(A) = \frac{i}{\pi} \int_{-\infty}^{\infty} \frac{e^{-t^2}}{A - t} dt \qquad Im(A) > 0 \qquad (6)$$

where Im(A) represents the imaginary part of the complex number A.

The input for the formulation outlined above is the geometry of a source/receiver combination, the frequency, the constant a, and the normalized acoustic admittance of the ground. A two-parameter model given by Delany and Bazley (ref. 5) was used to describe the normalized acoustic admittance. The two-parameter model given in a dimensionless form after Zorumski (ref. 8) is

$$v = \frac{\rho_0 c_0}{2} = \left[1 + (6.86\eta)^{-0.75} + (4.36\eta)^{-0.73}\right]^{-1}$$
 (7)

where ρ_O and c_O are the ground-level density and the speed of sound, respectively, z is the acoustical impedance, and η is given by

$$\eta \equiv \pi \rho_{O} f/\sigma$$
 (8)

where f is the frequency and σ is the ground flow resistance. A rough range of the value of σ for commonly encountered surfaces is from 750 Mg/(s-m³) for an acoustically hard surface to 50 Mg/(s-m³) for an acoustically soft surface.

Equation (1) is for discrete frequency prediction of ground effects. The acoustic data have been analyzed with 1/3-octave band analysis techniques. To make predictions comparable to the results of the 1/3-octave band analysis of the data, equation (1) must be changed to incorporate 1/3-octave band averaging. If the assumption is made that the complex reflection coefficient and the coherence factor vary little within a 1/3-octave band, the integration of equation (1) over a 1/3-octave band reduces to the integration of the cosine term. The integration yields

$$\frac{p^2}{p_0^2} = 1 + 2R \exp(-ak \Delta r)^2 \frac{\cos (\alpha + k_0 \Delta r) \sin (0.115k_0 \Delta r)}{0.115k_0 \Delta r}$$
(9)

where ko is the wave number of the 1/3-octave bandcenter frequency.

RESULTS

Variation With Frequency

Results of the near/far comparison method are compared with predictions in the frequency domain in figure 11. Results are presented for microphones 4, 6, 8, and 11, representing a lateral distance from the flight track ranging from 460 m to 1650 m, and for a subset of the ten "best" runs (runs 24, 21, 17, 27 and 26) which correspond to one flight for each altitude flown. The same run sequence will be used for all of the results to be given. The microphones were all 1.2-m microphones positioned over grass.

The geometry between the airplane and the measurement microphones at the calculated emission times was entered into the prediction procedure. The values assigned to the ground flow resistance and the constant a were optimized for the best agreement between theory and experiment. The range of values tried was from 30 to 500 Mg/(s-m 3) for ground flow resistance and from 0 to 1 for the constant a. The smallest standard error between the measured and predicted results was obtained with a value of 62.5 Mg/(s-m 3) for the ground flow resistance of grass and a value of 0.1 for a.

Plotted along the ordinate in figure 11 is ground attenuation in decibels (dB) and along the abscissa is frequency in Hz. The data are cut off at 2 kHz because the signal-to-noise ratio for higher frequencies was poor for the microphones positioned far from the flight track. The solid curves are the measured results, and the dashed lines are the predicted curves. The legend to the right of each plot identifies the run and measurement microphone as well as the slant range (SR) and the elevation angle β from the aircraft to the microphone at the emission time. (See fig. 9.) The plots in the figure are grouped according to the altitudes of the runs, beginning with the highest altitude run in figure 11(a) and ending with the lowest altitude run in figure 11(e).

As the measurement microphones get farther away from the flight track (as microphone number increases), the measured excess attenuation generally increases for a particular run in figure 11. Also, greater excess attenuations are observed for a particular microphone for the lower altitude flights. Restated, a trend of greater ground attenuation for smaller β is generally observed in the plots. The largest values of excess attenuation, greater than 20 dB, are found in the frequency range of 200 to 400 Hz. The agreement between the predicted frequency dependence and the measured dependence is good, while the predicted curves generally fall beneath the measured curves.

Results for the direct comparison method, along with predictions, are illustrated in figure 12 in a fashion similar to that presented for the near/far method. Results are given for the same run sequence as in the near/far method for microphone pairs 2-14 and 9-19, representing lateral distances from the flight track of 250 m and 1600 m, respectively. The predictions were made by computing ground effects spectra for each microphone of a pair and then subtracting the spectrum of the microphone over grass from the spectrum of the microphone over concrete. The values of the input parameters pertaining to the grass were the same as those selected to make the near/far comparison predictions, namely a value of 62.5 Mg/(s-m³) for the ground flow resistance of grass and a value of 0.1 for a. A range of values from 125 to 1000 Mg/(s-m³) was tried for the ground flow resistance of concrete. The smallest standard error of estimate was obtained between the measured and predicted results with a value of 750 Mg/(s-m³) for the ground flow resistance of concrete, and hence, this value was used in the predictions of figure 12.

The same general trends are observed in the direct comparison results as in the near/far comparison results: increased measured attenuation with decreasing β and maximum attenuation frequency in the range of 200 to 400 Hz. However, the measured spectra are more erratic than those obtained from the near/far method, and the predicted frequency of maximum attenuation is generally lower than the measured frequency. The direct comparison results are, in general, more complicated and not as easy to interpret as the near/far results. The direct comparison results represent the difference in ground effects between two locations, while the near/far results represent the absolute ground effects for one microphone location. From a prediction viewpoint, direct comparison predictions are also more complex and subject to larger errors, since errors in the two predicted ground effects spectra may be amplified when the spectra are subtracted.

Variations With Elevation Angle

Plotted in figure 13 are the measured and predicted excess ground attenuations obtained by the near/far comparison method given as a function of elevation angle β for the four 1/3-octave bands of center frequencies: 100, 250, 500, and 1000 Hz. Illustrated in the figure are results for all of the 1.2-m microphones over grass for the same run sequence as the earlier results. The excess ground attenuation results are divided into four slant-range groups: 230, 440, 900, and 1600 m. The average deviation of the slant range of a data point in a particular slant-range group is less than 10 percent. Division of the data by the chosen slant ranges partitions the data into the following

microphone combinations; 2, 4, 5-6-7, and 8-9-11, respectively. Plotted along the abscissa in each figure is β in degrees, ranging from 0.5 to 40; along the ordinate, ground attenuation in decibels. The measured results are denoted in the figure by the symbols; the dashed lines are the predictions.

Although scatter is evident in the measured results, similar trends are seen in the predicted results. The measured and predicted attenuations generally show a rapid decrease, approaching zero, with increasing β larger than 10° to 15° . The predicted curves generally fall beneath the majority of the data points.

Comparison of predictions with results from the direct comparison method for all the applicable 1.2-m microphone pairs for the same run sequence are given in figure 14 as a function of β . The results have been separated into a 230-m slant-range group and a 1600-m slant-range group. The average deviation of the slant range of a data point in a particular slant-range group is less than 10 percent. Results for microphone pair 2-14 are in the shorter slant-range group while the results from microphone pairs 8-18, 9-19, and 11-20 fall in the longer slant-range group. The large scatter and lack of trend seen in these plots, particularly in the 1600-m slant-range group, indicate the difficulty and complexity in the direct comparison method with respect to the near/far method in measuring excess ground attenuation.

Integrated Measure of Excess Ground Attenuation

An integrated noise metrics analysis was applied to the T-38A acoustic data base. Effective perceived noise level (EPNL) was calculated for a number of runs and microphones, and a measure of lateral attenuation in terms of EPNL units was determined using the near/far comparison method. The measurement microphones used were the 1.2-m microphones positioned over grass. The results of the EPNL calculations for the same run sequence as the results given before are illustrated in figure 15. Plotted along the ordinate is lateral attenuation in EPNL (dB) and along the abscissa is elevation angle β in degrees. Elevation angle is redefined for the integrated measures to be the angle between the source and the receiver at the point of closest approach. A 20 decibel spread is seen in the data for small elevation angles. Even with the spread, the trend observed earlier of increasing attenuation with decreasing elevation angle is clearly seen in the data. The corresponding closest-approach slant ranges associated with the data points plotted in figure 15 vary from 180 m to 1530 m.

The data from figure 15 have been subdivided and replotted in four slant-range groups: 190, 370, 765, and 1330 m. The average deviation of the slant range of a data point in a particular slant-range group is less than 10 percent. A third-order least-square fit, constrained to be zero at an elevation angle of 90 degrees, has been calculated for each slant-range group and plotted in figure 16 along with a lateral attenuation curve obtained from flight data gathered by Cooper (ref. 21). As a result of the subdivision into slant-range groups, a family of lateral attenuation curves is formed, and a slant-range dependence may be observed. As slant range decreases, less lateral attenuation is measured for the same elevation angles. For large elevation angles, the curves (or the extensions of the curves) merge, showing little measured attenuation. The two

largest slant-range curves collapse together on top of the curve for small elevation angles determined by Cooper. The slant ranges of the small elevation angle data of the curve in reference 21 were greater than 1330 m.

CONCLUDING REMARKS

Ground effects on aircraft noise were measured in a flight experiment over a wide range of elevation angles and slant ranges. A theoretical model chosen for comparison adequately predicted the measured ground effects on actual aircraft noise. Owing to the use of an airplane and practical propagation conditions, the results of the investigation are directly applicable to aircraft noise propagation problems.

The ground attenuation values were determined with two analysis methods; the near/far method and the direct comparison method. Results from the two methods agreed in general but exhibited considerable scatter, particularly for the direct comparison method which was found to be the inferior of the two methods. The scatter was due to many contributing factors, including atmospheric parameter gradients and fluctuations, the data sampling rate in the data reduction, and the finite dimensions of the test surfaces. Different atmospheric conditions over the grass and the runway were an additional factor contributing to the scatter in the direct comparison results.

The theoretical model employed was the ground effect prediction procedure recommended by Pao, Wenzel, and Oncley. The agreement between the measured and predicted results was good considering an outdoor environment, a moving noise source, and the long slant ranges. The predicted frequency of maximum ground attenuation agreed very well with the measured frequency, particularly for the near/far comparison results. The amplitudes of the predicted ground attenuation were generally smaller than the measured amplitudes.

The largest ground attenuations, in excess of 20 dB, were found for the 1/3-octave bands in the frequency range of 200 to 400 Hz. The measured ground attenuation quickly diminished with increasing elevation angle β . The measured ground attenuations were close to zero for β greater than 10° to 15°. A strong dependence of ground attenuation on slant range was observed, particularly in the effective perceived noise level results for small slant ranges. The farther the receiver was from the aircraft, the greater the measured ground attenuation for the same β . This slant-range dependence disappeared for slant ranges greater than about 750 m.

Langley Research Center National Aeronautics and Space Administration Hampton, VA 23665 October 27, 1980

APPENDIX A

FLIGHT DATA

Listed herein are the emission (EMIT) time, the emission position coordinates (X,Y,Z), the velocity (VEL), and the magnetic heading of the aircraft at the emission time. Emission times were calculated using a directivity angle criteria of 122.5°. Data are listed for every microphone and for every run. The data for a particular run and microphone are identified with the following nomenclature EGFR ##.M**, where ## is the run number and ** is the microphone number.

DIRECTIVITY	ANGLE =	122,5 de	e g			
FILENAME	EMIT	x	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFRØ1.MØ1	11:46:38.07	-31.1	50,0	11.9	89.6	99.6
EGFRØ1.MØ2	11:46:38.07	-31.1	50.0	11,9	89,6	99.6
EGFR01, M03	11:46:38.07	-31.2	50.1	11.9	89.6	99.6
EGFRØ1.MØ4	11:46:38.11	-29.2	46.9	11.9	89.6	99.6
EGFRØ1.M05	11:46:38.16	-26.5	42.5	11.9	89.6	99.6
EGFRØ1.MØ6	11:46:37.86	-41.1	66.1	11.9	89,6	99.6
EGFRØ1.M07	11:46:37,90	=39.Ø	62.8	11.9	89.6	99.6
EGFR01.M08	11:46:37,95	-36.8	59.3	11.9	89.6	99.6
EGFR01.M09	11:46:37.99	-34.8	56.0	11.9	89.6	99.6
EGFR01, M10	11:46:38.04	=32.6	52,4	11.9	89.6	99.6
EGFR01.M11	11:46:38.04	-32.6	52.4	11.9	89.6	99.6
EGFR01,M12	11:46:38.04	-32.6	52.3	11.9	89.6	99.6
EGFRU1.M18	11:46:39.00	12,5	-20.7	12.0	89.6	99.6
EGFRØ1.M19	11:46:39.04	14.5	-24.0	12.0	89.6	99.6
EGFRØ1.M29	11:46:39.09	16.7	-27.6	12.0	89,6	99.6

APPENDIX A

DIRECTIVITY ANGLE = 122,5 deg

FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR02, MØ1	11:54:27.57	=27.4	50.0	11.8	88,5	99.6
EGFRØ2.MØ2	11:54:27.57	-27.3	50.0	11.8	88.5	99.6
EGFR02.M03	11:54:27.57	-27.4	50.1	11.8	88.5	99.6
EGFR02.M04	11:54:27.61	-25,4	46,8	11.8	88.5	99.6
EGFRØ2. MØ5	11:54:27.67	-22.8	42.5	11.8	88.5	99.6
EGFRM2.MØ6	11:54:27.36	-37.3	66.1	11.8	88.5	99.6
EGFRØ2.MØ7	11:54:27.40	-35.3	62.8	11.8	88,5	99.6
EGFR02.M08	11:54:27.45	-33.1	59.2	11.8	88.5	99.6
EGFRØ2.M09	11:54:27.49	-31,1	56.0	11.8	88.5	99.6
EGFR02.M10	11:54:27.54	-28.9	52.4	11.8	88.5	99.6
EGFRØ2, M11	11:54:27.54	-28,8	52.4	11.8	88.5	99.6
EGFR02.M12	11:54:27.54	-28.8	52.3	11.8	88,5	99.6
EGFRØ2.M13	11:54:28.29	5.8	-3.8	11.9	88,5	99.6
EGFR02.M14	11:54:28.29	5.8	-3. 9	11.9	88.5	99.6
EGFRØ2.M15	11:54:28.28	5.8	-3.8	11.9	88.5	99.6
EGFRM2.M16	11:54:28.29	6.0	-4.2	11.9	88.5	99.6
EGFRØ2,M17	11:54:28,29	6.2	-4.5	11.9	88.5	99.6
EGFRØ2.M18	11:54:28.51	16.2	-20.7	11.9	88.5	99.6
EGFRAZ.M19	11:54:28.55	18.2	-24.0	11.9	88,5	99.6
EGFRØ2.M2Ø	11:54:28.60	20.5	-27.6	11.9	88.5	99.6

APPENDIX A

DIRECTIVITY	ANGLE =	122.5 deg
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FILENAME	EMIT	x	Y	Z	VEL.	HEADING
	TIME		(m)		(m/s)	(deg)
EGFRØ3.MØ1	11:58:54,52	- 29.8	49,3	11.9	89.4	99.7
EGFRØ3.MØ2	11:58:54.52	-29.8	49,3	11.9	89,4	99.7
EGFRØ3, MØ3	11:58:54.52	-29.9	49.4	11.9	89,4	99.7
EGFR03, M04	11:58:54,57	-27.5	45,5	11.9	89,4	99.7
EGFRØ3.MØ5	11:58:54.64	-24.3	40.2	11.9	89.4	99.7
EGFRØ3.MØ6	11:58:54.34	-38.4	63.3	11.9	89,4	99.7
EGFR03. M07	11:58:54,39	-36.0	59.3	11.9	89.4	99.7
EGFR03.M08	11:58:54.45	-33.3	55.0	11.9	89.4	99.7
EGFRØ3, MØ9	11:58:54.50	-30.9	51.0	11.9	89.4	99.7
EGFR03,M10	11:58:54.55	-28.2	46.7	11.9	89.4	99.7
EGFR03.M11	11:58:54.55	-28,2	46.6	11.9	89.4	99.7
EGFRØ3.M12	11:58:54.55	-28.2	46.6	11.9	89.4	99.7
EGFRØ3.M13	11:58:55,23	3,2	-4.6	11.9	89,4	99.7
EGFR03.M14	11:58:55.23	3,2	=4.6	11.9	89.4	99.7
EGFRØ3.M15	11:58:55,23	3.1	-4.5	11.9	89.4	99.7
EGFRØ3.M16	11:58:55,24	3.7	-5.4	11.9	89.4	99.7
EGFRØ3, M17	11:58:55.24	3.8	-5.6	11.9	89.4	99.7
EGFRØ3.M18	11:58:55.50	15.7	-25,2	11.79	89.4	99.7
EGFR03.M19	11:58:55.55	18.4	-28.9	11.9	93,2	96.2
EGFR03.M20	11:58:55,60	21.4	-33,2	11.9	93.2	96,2

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg	1			
FILENAME	EMIT	X	· Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFRØ4, MØ1	12: 2:47.68	-40.6	46.5	12.9	89.2	100.6
EGFRØ4.MØ2	12: 2:47.68	-40.6	46.4	12.9	89.2	100.6
EGFRØ4.MØ3	12: 2:47.68	-40.7	46.5	12.9	89.2	100.6
EGFRØ4.MØ4	12: 2:47.78	3 -36.4	39.4	12.9	89.2	100.6
EGFR04.M05	12: 2:47.98	3 -30.7	29.8	12.9	89.2	100.6
EGFRØ4.MØ6	12: 2:47.63	3 -43.0	50.5	12,9	89.2	100.6
EGFRØ4.MØ7	12: 2:47.73	3 -38.7	43.2	12,9	89.2	100.6
EGFRØ4.MØ8	12: 2:47.83	3 =34,0	35.2	12.9	89.2	100.6
EGFR04, M09	12: 2:47.9	3 -29.7	28.0	12.9	89.2	100.6
EGFRØ4, M10	12: 2:48.0	3 -25,0	20.0	12.9	91.1	100.9
EGFRØ4.M11	12: 2:48.0	3 =24.9	19.9	12.9	91.1	100.9
EGFRØ4.M12	12: 2:48.0	3 -24.9	19.8	12.9	91.1	100.9
EGFRØ4, M13	12: 2:48.3	8 -8.6	-7,9	12.5	91.1	100.9
EGFRØ4.M14	12: 2:48,3	8 -8,6	-8.0	12.5	91.1	100.9
EGFRØ4.M15	12: 2:48.3	8 -8,6	-7.9	12,5	91.1	100.9
EGFRØ4.M16	12: 2:48.4	7 -4.7	-14.6	12.4	91.1	100.9
EGFRØ4.M17	12: 2:48.4	7 -4.6	-14.8	12.4	91.1	100.9
EGFRØ4.M18	12: 2:48.9	7 18.2	*53. 8	11.8	91.1	109.9
EGFR04.M19	12: 2:49.0	7 23.2	-62.3	11.6	91.1	100.9
EGFRØ4.M2Ø	12: 2:49.2	g 28.8	-71.9	11.5	91.1	100.9

, APPENDIX A

DIRECTIVITY ANGLE = 1	22	. 5	deg
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FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(dea)
EGFRØ5.MØ1	12: 6:59,17	-23,8	50.8	12.4	91,8	99.3
EGFR05,M02	12: 6:59,17	-23.8	50.8	12,4	91,8	99.3
EGFRØ5, MØ3	12: 6:59.17	-23.9	50.9	12.4	91.8	99.3
EGFRØ5, MØ4	12: 6:59.20	-22.4	48.5	12.4	91.8	99.3
EGFRØ5, MØ5	12: 6:59,24	-20,5	45.4	12.4	91.8	99.3
EGFRØ5, MØ6	12: 6:58,93	-35.6	69.7	12.4	91.8	99.3
EGFRØ5.MØ7	12: 6:58.96	-34.1	67.3	12.4	91.8	99.3
EGFRØ5.MØ8	12: 6:59.00	-32,5	64.7	12.4	91.8	99.3
EGFRØ5, MØ9	12: 6:59.02	-31.0	62.3	12.4	91.8	99.3
EGFRØ5.M10	12: 6:59,06	-29.4	59.7	12.4	91.8	99.3
EGFRØ5.M11	12: 6:59.06	-29.4	59.7	12.4	91.8	99.3
EGFRØ5, M12	12: 6:59.06	-29.3	59.7	12.4	91.8	99.3
EGFR05.M13	12: 6:59,86	9.6	-2.9	12,4	91.8	99.3
EGFR05. M14	12: 6:59.86	9.6	-2.9	12.4	91.8	99.3
EGFRØ5.M15	12: 6:59,86	9,5	-2.8	12.4	91.8	99.3
EGFRØ5, M16	12: 6:59,87	9.8	-3. 3	12.4	91.8	99.3
EGFRØ5.M17	12: 6:59,87	10.0	-3,6	12,4	91.8	99.3
EGFRØ5.M18	12: 7: 0.02	17.2	-15.1	12.4	91.8	99.3
EGFRØ5.M19	12: 7: 0.05	18.6	-17.4	12.4	91.8	99.3
EGFRØ5, M20	12: 7: 0.08	20.3	-20.1	12.4	91.8	99.3

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg
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FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFRØ6.MØ1	19:37:37,79	-24,5	51,8	13.1	90.7	99.0
EGFRØ6 MØ2	19:37:37.79	=24.5	51.8	13.1	90.7	99.0
-					-	_
EGFRØ6.MØ3	19:37:37.79	=24,6	52.0	13.1	90.7	99.0
EGFRØ6.MØ4	19:37:37:80	~23.7	50.7	13.1	90.7	99.0
EGFRØ6, MØ5	19:37:37.83	-22.7	49.0	13.1	90.7	99.0
EGFRØ6. MØ6	19:37:37.50	-38.4	74.0	13.1	90.7	99.0
EGFRØ6.MØ7	19:37:37,52	=37.6	72.7	13.1	90.7	99.0
EGFRØ6, MØ8	19:37:37.53	=36.7	71.3	13,1	90.7	99.0
EGFRØ6.MØ9	19:37:37.55	-35,9	70.0	13.1	90.7	99.0
EGFRØ6.M1Ø	19:37:37.45	-13.4	80.5	17.0	86.4	105.5
EGFRØ6.M11	19:37:37:45	-13,4	80.5	17.0	86,4	105.5
EGFRØ6.M12	19:37:37.45	=13.4	80.5	17.0	86,4	105.5
EGFRØ6.M13	19:37:38.48	9.2	-1.7	13.2	90.7	99.0
EGFRØ6.M14	19:37:38.48	9.2	-1.7	13.2	90.7	99.0
EGFRØ6.M15	19:37:38.48	9.1	-1.5	13,2	90.7	99.0
EGFRØ6.M16	19:37:38,51	10.3	- 3,5	13.2	90.7	99.0
EGFRØ6.M17	19:37:38.52	10.5	-3.8	13.2	90.7	99.0
EGFRØ6.M18	19:37:38,57	13.3	-8.3	13.2	90.7	99.0
EGFRØ6, M19	19:37:38.59	14.1	-9.5	13.2	90.7	99.0
EGFRØ6, M20	19:37:38.61	15.0	-11.0	13.2	90.7	99.0

APPENDIX A

DIRECTIVITY ANGLE = 122.5 deg

FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFRØ7.MØ1	19:42:47,95	-28,7	50.8	6.9	92,8	99.4
EGFR07.MØ2	19:42:47.95	-28,7	50.8	6.9	92.8	99.4
·	-				_	
EGFRØ7.MØ3	19:42:47,95	-28.7	50.8	6.9	92.8	99.4
EGFRØ7.MØ4	19:42:47.98	-27.2	48.4	6.9	92,8	99,4
EGFRØ7.MØ5	19:42:48.02	-25.1	45.0	6.9	92.8	99.4
EGFRØ7.MØ6	19:42:47.72	-40.1	69.2	6.9	92.8	99.4
EGFRØ7.MØ7	19142147.75	-38.5	66.6	6.9	92.8	99.4
EGFRØ7.MØ8	19:42:47.78	-36 8	63.9	6.9	92,8	99.4
EGFRØ7.MØ9	19:42:47.82	-35,3	61.4	6.9	92.8	99.4
EGFRØ7, M10	19:42:47.85	-33,6	58.6	6.9	92.8	99.4
EGFRØ7.M11	19:42:47.85	-33,5	58.6	6.9	92.8	99.4
EGFR07.M12	19:42:47.85	*33.5	58.5	6.9	92.8	99.4
EGFR07, M13	19:42:48.63	4.6	-2.9	6.9	92.8	99.4
EGFRØ7.M14	19:42:48.63	4.7	-2.9	6.9	92.8	99.4
EGFRØ7.M15	19:42:48.63	4.6	-2.9	6.9	92.8	99.4
EGFRØ7, M16	19:43: 3.66	-181.9-1	1885.2	-384.3	102.1	71.9
EGFR07.M17	19:43: 3.66	-181.9-1	1882.3	-384.3	102,1	71.9
EGFRØ7.M18	19:42:48.80	12.8	-15.9	6.9	92.8	99.4
EGFR07.M19	19:42:48.83	14.3	-18.4	6.9	92.8	99.4
EGFR07, M20	19:42:48.87	16.0	-21.2	6.9	92.8	99.4

APPENDIX A

DIRECTIVITY	ANGLE = 1	22,5 de	g			
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)	·	(m/s)	(deg)
	A					
EGFRØ8.MØ1	19:48:45.80	-30.0	50.5	8.3	93,6	99.4
EGFRØ8, MØ2	19:48:45.80	~30.0	50.5	8.3	93,6	99.4
EGFRØ8.MØ3	19:48:45.79	-30,0	50.5	8.3	93.6	99.4
EGFRØ8.MØ4	19:48:45.83	=28.3	47.7	8.3	93.6	99.4
EGFRØ8, MØ5	19:48:45.88	-26.0	44.0	8.3	93,6	99.4
EGFRØ8, MØ6	19:48:45.58	-40,8	67.9	8.3	93.6	99.4
EGFRØ8.MØ7	19:48:45.61	-39.0	65.0	8,3	93.6	99.4
EGFRØ8.MØ8	19:48:45.65	-37.1	61.9	8.3	93.6	99.4
EGFR08, M09	19:48:45.69	-35,3	59.1	8.3	93,6	99.4
EGFRØ8.M1Ø	19:48:45.73	-33.4	55.9	8.3	93,6	99,4
EGFR08,M11	19:48:45.73	-33.4	55.9	8.3	93,6	99.4
EGFRØ8,M12	19:48:45.73	-33.3	55.9	8.3	93.6	99.4
EGFRØ8,M13	19:48:46.47	3.3	-3.3	8.3	93,6	99.4
EGFRØ8.M14	19148146.47	3.3	-3.3	8.3	93.6	99.4
EGFRØ8, M15	19148146,47	3.3	-3,2	8.3	93.6	99.4
EGFRØ8.M16	19:48:46.47	3.2	*3.1	8.3	93.6	99.4
EGFR08, M17	19:48:46,47	3,3	-3.3	8.3	93.6	99.4
EGFRØ8.M18	19:48:46.66	12.4	=18.0	8.3	93.6	99.4
EGFRØ8, M19	19:48:46.69	14.1	-20.8	8.3	93.6	99.4

EGFR08, M20 19:48:46.73 16.1 -24.0 8.3 93.6 99.4

APPENDIX A

DIRECTIVITY	ANGLE =	122.5 deg	3			
FILENAME	EMIT	×	Y	Z	VEL	HEADING
***********	TIME		(m)		(m/s)	(deg)
EGFRØ9, MØ1	19:52:38,40	-28.9	50.1	5.7	93,4	99.6
EGFRØ9.MØ2	19:52:38.40	-28,9	50.1	5.7	93.4	99.6
EGFRØ9.MØ3	19:52:38,40	-28.9	50.1	5.7	93.4	99.6
EGFRØ9.MØ4	19:52:38.44	- 26,9	46.9	5.7	93.4	99.6
EGFRØ9, MØ5	19:52:38.49	=24.3	42.6	5.7	93.4	99.6
EGFRØ9, MØ6	19:52:38:20	=38 ,8	66.2	5.7	93.4	99.6
EGFRØ9.MØ7	19:52:38.23	-36,8	62.9	5.7	93.4	99,6
EGFRØ9. MØ8	19152138,28	=34.6	59.4	5.7	93.4	99.6
EGFR09.M09	19:52:38.32	-32,6	56.1	5.7	93.4	99.6
EGFRØ9.M10	19:52:38.37	-30,4	52.5	5.7	93.4	99.6
EGFRØ9.M11	19452138.37	-30.4	52.5	5.7	93.4	99.6
EGFRØ9,M12	19:52:38.37	-30.4	52.5	5.7	93.4	99.6
EGFRØ9.M13	19:52:39.08	4.3	-3.7	5.6	93,4	99.6
EGFRØ9.M14	19:52:39.08	4.3	-3.7	5,6	93,4	99.6
EGFRØ9.M15	19:52:39,08	4.3	-3.7	5.6	93,4	99.6
EGFRØ9, M16	19:52:39.05	2.9	-1.4	5,6	93.4	99.6
EGFRØ9, M17	19:52:39.05	3.0	-1,7	5.6	93.4	99.6
EGFRØ9.M18	19152138.53	*3 6	44.4	9,9	90.3	104.6
EGFR09, M19	19:52:39,33	16.7	-23.8	5.5	93.4	99.6
EGFRØ9.M20	19:52:39.38	18.9	-27.5	5.5	93.4	99.6

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg				
FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
	40.54.3/ 1//	-27.2	50.7	18.5	93.4	99.3
EGFR10, M01	19:56:24.14			·	93.4	99.3
EGFR10.M02	19:56:24.14	•27.2	50.7	18.5	-	•
EGFR10.M03	19:56:24.13	-27.4	51.0	18.5	93.4	99.3
EGFR10.M04	19:56:24.16	= 26.0	48.7	18.5	93.4	99,3
EGFR10.M05	19:56:24.20	-24.2	45.8	18.5	93.4	99.3
EGFR10.M06	19:56:23.89	-39. 4	70.2	18.5	93.4	99.3
EGFR10.M07	19156123.92	=37,9	67.9	18.5	93.4	99.3
EGFR10, M08	19:56:23.95	-36.4	65.5	18.5	93.4	99.3
EGFR10.M09	19:56:23.98	-35,1	63.3	18.5	93,4	99.3
EGFR10.M10	19:56:24.02	=33.5	60,8	18.5	93.4	99,3
EGFR10.M11	19:56:24.02	*33.5	60.8	18.5	93.4	99,3
EGFR10.M12	19:56:24.02	*33.5	60.8	18.5	93.4	99.3
EGFR10.M13	19156124.82	6.2	-2.9	18.6	93.4	99.3
EGFR10,M14	19:56:24.82	6.2	-2.9	18.6	93.4	99.3
EGFR10.M15	19156124,81	6.0	-2.7	18.6	93.4	99.3
EGFR10.M16	19156124.88	9.0	-7.4	18.6	93.4	99.3
EGFR10.M17	19156124.88	9.1	-7.6	18.6	93,4	99.3
EGFR10.M18	19156124.96	13.2	-14.2	18.6	93.4	99.3
EGFR10.M19	19:56:24.98	14.6	-16.5	18.6	93.4	99.3
EGFR10.M20	19:56:25.02	16.2	-18,9	18.6	93.4	99.3

APPENDIX A

DIRECTIVITY	ANGLE	=	122.5 de	19			
FILENAME	EMI	T	x	Y	Z	VEL	HEADING
	TIM	E		(m)		(m/s)	(deg)
505044 May						******	
EGFR11.M01	20: 0:	2.09	-33 ,9	48.5	21.2	94.1	99.9
EGFR11.MØ2	20: 0:	2.09	- 33,9	48.5	21.2	94.1	99.9
EGFR11, MØ3	20: 0:	2.09	-34.1	48.8	21.2	94.1	99.9
EGFR11.MØ4	20: 0:	2.14	-31,4	44.4	21.2	94.1	99.9
EGFR11.M05	20: 0:	2 . 2.1	-27.9	38.7	21.1	94.1	99.9
EGFR11, MØ6	20: 0:	1.92	-41.8	61.5	21.2	94,1	99.9
EGFR11.MØ7	50: 0:	1.98	-39.1	57.0	21.2	94.1	99.9
EGFR11.MØB	20: 0:	2.04	~36.1	52.2	21.2	94.1	99.9
EGFR11.M09	20: 0:	2.09	-33.5	47.8	21.2	94.1	99.9
EGFR11.M1Ø	20: 0:	2.16	-30,5	42.9	21.2	94.1	99.9
EGFR11.M11	20: 0:	2.16	-30.5	42.9	21.2	94.1	99.9
EGFR11.M12	20: 0:	2,16	=30 a 4	42.9	21.2	94.1	99.9
EGFR11,M13	20: 0:	2.76	-1.0	-5.4	21.1	94.1	99.9
EGFR11.M14	20: 0:	2.76	-1.0	-5.4	21.1	94.1	99.9
EGFR11.M15	20: 0:	2,76	-1.2	-5.1	21.1	94.1	99.9
EGFR11,M16	20: 0:	2.85	3,4	-12.7	21.1	94,1	99.9
EGFR11.M17	20: 0:	2.85	3,6	-12.9	21.1	94.1	99.9
EGFR11,M18	20: 0:	3.04	12.8	-28.0	21.1	94.1	99.9
EGFR11.M19	20: 0:	3.09	15.4	-32.4	21.1	94.1	99.9
EGFR11, M20	20: 0:	3.16	18.4	-37.3	21.1	94.1	99,9

APPENDIX A

DIRECTIV	ITY ANGLE	= 122	,5 deg
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FILENAME	EMIT	x	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR12, MØ1	20: 3:59.09	-29. 2	50.1	22,3	95,4	99.4
EGFR12.MØ2	20: 3:59.09	- 29,2	50.1	22.3	95,4	99.4
EGFR12.M03	20: 3:59.09	-29.5	50.5	22.3	95,4	99.4
EGFR12.M04	20: 3:59.13	~27.8	47.8	22.3	95.4	99.4
EGFR12.MØ5	20: 3:59,16	-25.7	44.4	22.3	95.4	99.4
EGFR12, MØ6	20: 3:58,87	-40.7	68.5	22.3	95.4	99.4
EGFR12.MØ7	20: 3:58.90	-39.0	65.9	22.3	95,4	99.4
EGFR12, MØ8	20: 3:58.94	-37.2	63.0	22.3	95,4	99.4
EGFR12.MØ9	20: 3:58.97	* 35.6	60.4	22.3	95.4	99.4
EGFR12,M10	20: 3:59.01	=33.8	57.5	22.3	95.4	99.4
EGFR12.M11	20: 3:59.01	-33. 8	57.4	22.3	95.4	99.4
EGFR12.M12	20: 3:59.01	-33.8	57.4	22.3	95.4	99.4
EGFR12.M13	20: 3:59.76	4.1	-3.6	22,4	95.4	99.4
EGFR12,M14	20: 3:59.76	4.0	-3.5	22.4	95.4	99.4
EGFR12.M15	20: 3:59.75	3.9	-3.2	22.4	95.4	99.4
EGFR12.M16	20: 3:59.84	8,3	-10.4	22.4	95.4	99.4
EGFR12,M17	20: 3:59.84	8.4	-10.6	22.4	95,4	99.4
EGFR12.M18	20: 3:59,92	12.3	-16.8	22.4	95.4	99.4
EGFR12.M19	20: 3:59.95	13.9	-19.5	22.4	95,4	99.4
EGFR12,M20	201 3159,99	15,7	-22.4	22.4	95.4	99.4

APPENDIX A

DIRECTIVITY ANGLE = 122.5 deg

FILENAME	EMIT	×	Y	Z	VEL.	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR13.MØ1	21: 2:30.94	-39,9	45.9	19.6	102.5	100.6
EGFR13.MØ2	21: 2:30.04	-39.9	45.9	19.6	102.5	100.6
EGFR13.MØ3	21: 2:30.04	-40.0	46.1	19.6	102.5	100.6
EGFR13, M04	21: 2:30.13	-35.7	38.7	19.6	102.5	100.6
EGFR13.MØ5	21: 2:30,23	-29.8	28.8	19.6	102.5	100.6
EGFR13.MØ6	21: 2:30.00	-42.0	49.4	19,6	102.5	100.6
EGFR13, MØ7	21: 2:30.09	=37.4	41.8	19,6	102.5	100.6
EGFR13, MØ8	21: 2:30.18	*32.6	33.6	19.6	102.5	100.6
EGFR13.MØ9	21: 2:30.27	=28.2	26.1	19.6	102.5	100.6
EGFR13.M10	21: 2:30.36	-23.3	17.8	19.7	102,5	100.6
EGFR13.M11	21: 2:30,36	-23,2	17.7	19.7	102,5	100.6
EGFR13.M12	21: 2:30.36	-23.2	17.6	19.7	102.5	100.6
EGFR13,M13	21: 2:30.66	~7.8	-8.4	19.7	102.5	100.6
EGFR13,M14	21: 2:30,66	-7,8	-8. 5	19.7	102.5	100.6
EGFR13.M15	21: 2:30.66	= 7.9	-8.3	19.7	102.5	100.6
EGFR13.M16	21: 2:30,76	~ 2.6	-17.2	19.7	102.5	100.6
EGFR13.M17	21: 2:30.76	-2,5	-17.4	19.7	102.5	100.6
EGFR13,M18	21: 2:31.10	15.2	-47.3	19.8	102.5	100.6
EGFR13.M19	21: 2:31.18	19.6	- 54.7	19.8	102,5	100.6
EGFR13.M20	21: 2:31,28	24.5	-63.1	19.8	102.5	100.6

APPENDIX A

DIRECTIVITY ANGLE	= 122.5	5 deg
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FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	/ (deg)
EGFR14.MØ1	21: 6:19,05	-27.6	50.4	20.7	92,0	99.3
EGFR14, MØ2	21: 6:19.05	-27.6	50.5	20.7	92.0	99.3
EGFR14. M03	21: 6:19,05	-27.8	50.8	20.7	92.0	99.3
EGFR14. MØ4	21: 6:19.08	-26.3	48.4	20.7	92.0	99.3
EGFR14.MØ5	211 6119.12	-24.5	45.4	20.7	92.0	99.3
EGFR14. MØ6	21: 6:18,80	-39.6	69.7	20.7	92.0	99.3
EGFR14, MØ7	21: 6:18.84	-38,1	67.3	20.7	92.0	99.3
EGFR14, MØ8	21: 6:18,87	-36,5	64.8	20.7	92.0	99.3
EGFR14. MØ9	21: 6:18.90	*35,1	62.4	20.7	92.0	99.3
EGFR14.M1Ø	21: 6:18,93	-33.5	59.9	20.7	92,0	99.3
EGFR14, M11	21: 6:18.93	-33,4	59.8	20.7	92,0	99.3
EGFR14.M12	21: 6:18,93	-33,4	59.8	20.7	92,0	99.3
EGFR14,M13	21: 6:19.73	5,8	-3.2	20.7	92.0	99.3
EGFR14.M14	21: 6:19.73	5,8	-3.2	20.7	92.0	99.3
EGFR14.M15	211 6119.73	5,6	-2.9	20.7	92.0	99.3
EGFR14.M16	21: 6:19.80	9.2	-8.8	20.7	92,0	99.3
EGFR14.M17	21: 6:19,81	9.4	=9.Ø	20.7	92.0	99.3
EGFR14.M18	21: 6:19.89	13.1	=15.0	20.7	92.0	99.3
EGFR14.M19	21: 6:19.91	14.6	-17.3	20.7	92.0	99.3
EGFR14.M2Ø	21: 6:19.95	16.2	=19:9	20.7	92.0	99.3

APPENDIX A

DIRECTIVITY	ANGLE =	122.5 deg)		·	
FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)

EGFR15, MØ1	21: 9:53.39	-39.3	47.9	18.6	94.3	100.1
EGFR15. MØ2	21: 9:53.39	=39.3	47.9	18.6	94.3	100.1
EGFR15, MØ3	21: 9:53,39	-39.5	48.2	18.6	94.3	100.1
EGFR15, M04	21: 9:53.45	*36.3	42.9	18.6	94.3	100.1
EGFR15.M05	21: 9:53.54	-32.1	36,0	18.6	96.0	100.3
EGFR15.MØ6	21: 9:53.27	= 45.6	58.3	18.7	94.3	100.1
EGFR15, MØ7	21: 9:53.33	=42.3	53.0	18.7	94.3	100.1
EGFR15, MØ8	21: 9:53.40	-38.9	47.2	18.6	94.3	100.1
EGFR15, M09	21: 9:53.47	*35. 8	42.1	18.6	94.3	100.1
EGFR15.M10	21: 9:53.54	= 32 , 3	36.3	18.6	96.0	100.3
EGFR15.M11	21: 9:53.54	~ 32,2	36,2	18.6	96.0	100.3
EGFR15.M12	21: 9:53.54	-32,2	36,2	18.6	96.0	100.3
EGFR15.M13	21: 9:54,06	=6.4	-6.9	18.8	96.0	100.3
EGFR15.M14	21: 9:54.06	-6.4	-6.9	18.8	96.0	100.3
EGFR15, M15	21: 9:54.06	#6.5	-6.7	18.8	96.0	100.3
EGFR15, M16	21: 9:54.16	-1.4	-15.2	18.8	96.0	100.3
EGFR15.M17	21: 9:54.16	-1.3	-15.4	18.8	96.0	100.3
EGFR15,M18	21: 9:54.45	12.5	-38.4	18.9	96.0	100.3
EGFR15. M19	21: 9:54.52	16.1	-44.5	19.0	96.0	100.3
EGFR15, M20	21: 9:54.60	20,2	-51.3	19.0	96.0	100.3

APPENDIX A

DIRECTIVITY	ANGLE = 1	122.5 de	9			
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
		, . ,				
EGFR16.MØ1	21:13:54.52	=42.4	45.5	37.7	95.3	100.4
EGFR16, MØ2	21113154.52	-42.4	45.6	37.7	95.3	100.4
EGFR16.MØ3	21:13:54.52	-42.8	46.3	37.7	95.3	100.4
EGFR16.MØ4	21:13:54.59	-39.2	40.3	37.7	95.3	100.4
EGFR16.MØ5	21:13:54.69	-34.3	32.1	37.7	95.3	100.4
EGFR16.MØ6	21:13:54.42	-47.2	53.5	37.6	95.3	100.4
EGFR16, MØ7	21113154.50	-43.3	47.0	37.6	95, 3	100.4
EGFR16.MØ8	21:13:54.59	=39.1	40.1	37,7	95.3	100.4
EGFR16.MØ9	21:13:54.66	-35.3	33.7	37.7	95.3	100.4
EGFR16.M10	21:13:54.75	-31.1	26.6	37.8	95.3	100.4
EGFR16.M11	21:13:54.75	-31,0	26.5	37.8	95.3	100.4
EGFR16.M12	21:13:54.75	-31.0	26.5	37.8	95,3	100.4
EGFR16.M13	21:13:55.17	-10.1	~8,5	38.1	100.2	100.4
EGFR16. M14	21:13:55.17	-10.1	-8.5	38.1	100.2	100.4
EGFR16,M15	21:13:55,16	-10,5	-7.9	38.1	100.2	100.4
EGFR16.M16	21113:55.40	1.3	-27.7	38.5	100.2	100.4
EGFR16.M17	21:13:55.40	1.4	~27 ,9	38.5	100.2	100.4
EGFR16.M18	21:13:55,55	8.9	-40.2	38.7	96.5	98.7
EGFR16.M19	21:13:55,62	12,9	-46.5	38.8	96.5	98.7
EGFR16.M2Ø	21:13:56,52	56.0	-119.5	40.2	93.3	99.5

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg		•		
FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR17.M01	21:17:35,52	=33.3	47.4	39.3	96.3	99.7
EGFR17.MØ2	21:17:35.52	-33.4	47.5	39.3	96.3	99.7
EGFR17, MØ3	21:17:35.51	-33,9	48.3	39.3	96.3	99.7
EGFR17. M04	21:17:35,55	-31.8	44.9	39.2	96.3	99.7
EGFR17.M05	21:17:35.60	-29.0	40.4	39.2	96.3	99.7
EGFR17.MØ6	21:17:35,32	~43.4	63.8	39.3	96.3	99.7
EGFR17. M07	21:17:35,36	-41.1	60.1	39.3	96.3	99.7
EGFR17, MØ8	21:17:35.41	-38,7	56.1	39.3	96.3	99:47
EGFR17.MØ9	21:17:35.45	-36. 4	52.5	39.3	96,3	99.7
EGFR17.M10	21:17:35.51	=33,9	48.4	39.3	96.3	99.7
EGFR17.M11	21:17:35.51	~33 ,9	48.3	39,3	96.3	99.7
EGFR17,M12	21:17:35.51	~33.9	48.4	39.3	96.3	99.7
EGFR17.M13	21:17:36.17	-0.4	=6.2	39.1	96.3	99.7
EGFR17.M14	21:17:36:17	-0.5	-6.1	39.1	96.3	99.7
EGFR17.M15	21:17:36.16	-0.9	-5.4	39.1	96.3	99.7
EGFR17.M16	21:17:36.37	9,5	22.4	39.0	96.3	99.7
EGFR17.M17	21:17:36.37	9.7	22.6	39.0	96.3	99.7
EGFR17.M18	21:17:36.38	10.5	24.0	39.0	96.3	99.7
EGFR17, M19	21:17:36.43	12.7 -	27.6	39.0	96.3	99.7
EGFR17.M20	21:17:36.48	15.2	31.7	39.0	96.3	99.7

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg				
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)	_	(m/s)	(deg)
*=========				******		
EGFR18.MØ1	21:20:57.65	-31.0	47.3	37.8	96.9	99.7
EGFR18.MØ2	21:20:57.65	-31.0	47.4	37.8	96.9	99.7
EGFR18.MØ3	21:20:57.64	-31,5	48.2	37.8	96.9	99.7
EGFR18.M04	21:20:57.68	-29,3	44.6	37.8	96.9	99.7
EGFR18.M05	21:20:57.74	~26,5	39,9	37.7	96,9	99.7
EGFR18, MØ6	21:20:57.46	-40.7	63.2	37.9	96.9	99.7
EGFR18, M07	21:20:57.51	=38,4	59.4	37.9	96.9	99.7
EGFR18.MØ8	21:20:57.55	-35.9	55.3	37.8	96.9	99.7
EGFR18,M09	21:20:57.60	-33.6	51.5	37.8	96,9	99.7
EGFR18,M10	21:20:57.65	-31,0	47.3	37.8	96,9	99.7
EGFR18,M11	21:20:57.65	-31.0	47.3	37.8	96.9	99.7
EGFR18.M12	21:20:57.65	-31.0	47.4	37,8	96.9	99.7
EGFR18.M13	21:20:58.30	1.9	-6.3	37.4	96.9	99.7
EGFR18.M14	21:20:58.30	1.8	-6.2	37.4	96.9	99.7
EGFR18.M15	21:20:58.29	9 1.4	-5.6	37.4	96.9	99.7
EGFR18,M16	21120158.4	3 10.6	-20.6	37.3	96.9	99.7
EGFR18.M17	21:20:58.4	8 10.7	-20.8	37.3	96.9	99.7
EGFR18,M18	21:20:58.5	2 13.2	-24.8	37.3	96.9	99.7
EGFR18,M19	21:20:58.5	7 15.5	-28.6	37,2	96.9	99.7
EGFR18.M20	21:20:58.6	2 18.1	=32.8	37.2	96.9	99.7

APPENDIX A

DIRECTIVIT	Y ANGLE =	122,5 de	g			
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR19, MØ1	21:25:57.80	-35.8	41.8	70.4	98.2	99.9
EGFR19.MØ2	21:25:57.80	-36.0	42.1	70.4	98.2	99.9
EGFR19, M03	21:25:57.78	-36.9	43.6	70.4	98,2	99.9
EGFR19.MØ4	21:25:57.81	-35.4	41.1	70.4	98.2	99.9
EGFR19. M05	21:25:57.87	-32.5	36.4	70.4	98.2	99.9
EGFR19.MØ6	21:25:57.59	-46.5	59. _e 4	70.3	98,2	99.9
EGFR19.MØ7	21125157.64	-43.8	55.0	70.3	98.2	99.9
EGFR19. MØ8	21:25:57.70	-40.9	50.2	70.3	98.2	99.9
EGFR19. MØ9	21:25:57.75	-38.2	45.8	70.4	98.2	99,9
EGFR19.M10	21:25:57.81	-35,1	40.7	70.4	98.2	99,9
EGFR19.M11	21:25:57.81	-35,1	40.7	70.4	98.2	99.9
EGFR19.M12	21:25:57.81	-35,2	40,8	70.4	98.2	99.9
EGFR19,M13	21:25:58.43	•3.5	-11.3	70.6	98.2	99.9
EGFR19, M14	21:25:58.43	-3.7	-11.0	70.6	98.2	99,9
EGFR19,M15	21:25:58.41	-4.4	-9.7	70.6	98,2	99.9
EGFR19.M16	21:25:58.80	15.3	~42.3	70.7	98.2	99.9
EGFR19,M17	21:25:58,80	15.5	-42.5	70.7	98.2	99.9
EGFR19, M18	21125158.66	7.9	-30.0	70.6	98.2	99.9
EGFR19.M19	21:25:58.71	10.6	-34.5	70.7	98,2	99.9
EGFR19,M20	21:25:58.77	13.7	~39.6	70,7	98,2	99.9

APPENDIX A

EGFR20.M02 21:29:39.56 =32.3	
EGFR20.M01 21:29:39.57 -32.1 39.9 85.4 98.2 99 EGFR20.M02 21:29:39.56 -32.3 40.2 85.4 98.2 99 EGFR20.M03 21:29:39.55 -33.3 42.0 85.3 98.2 99 EGFR20.M04 21:29:39.55 -33.0 41.4 85.3 98.2 99 EGFR20.M05 21:29:39.59 -31.0 38.2 85.4 98.2 99 EGFR20.M06 21:29:39.30 -45.5 61.9 85.1 98.2 99 EGFR20.M07 21:29:39.35 -43.3 58.3 85.1 98.2 99 EGFR20.M08 21:29:39.40 -40.9 54.3 85.2 98.2 99	ING
EGFR20.M02 21:29:39.56 =32.3	g)
EGFR20.M02 21:29:39.56 =32.3	
EGFR20.M03 21:29:39.55 =33.3 42.0 85.3 98.2 99 EGFR20.M04 21:29:39.55 =33.0 41.4 85.3 98.2 99 EGFR20.M05 21:29:39.59 =31.0 38.2 85.4 98.2 99 EGFR20.M06 21:29:39.30 =45.5 61.9 85.1 98.2 99 EGFR20.M07 21:29:39.35 =43.3 58.3 85.1 98.2 99 EGFR20.M08 21:29:39.40 =40.9 54.3 85.2 98.2 99	7
EGFR20.M04 21:29:39.55 =33.0 41.4 85.3 98.2 99 EGFR20.M05 21:29:39.59 =31.0 38.2 85.4 98.2 99 EGFR20.M06 21:29:39.30 =45.5 61.9 85.1 98.2 99 EGFR20.M07 21:29:39.35 =43.3 58.3 85.1 98.2 99 EGFR20.M08 21:29:39.40 =40.9 54.3 85.2 98.2 9	7
EGFR20.M05 21:29:39.59 =31.0 38.2 85.4 98.2 99.2 EGFR20.M06 21:29:39.30 =45.5 61.9 85.1 98.2 99.2 EGFR20.M07 21:29:39.35 =43.3 58.3 85.1 98.2 99.2 EGFR20.M08 21:29:39.40 =40.9 54.3 85.2 98.2 9	7
EGFR20.M06 21:29:39.30 -45.5 61.9 85.1 98.2 9' EGFR20.M07 21:29:39.35 -43.3 58.3 85.1 98.2 9' EGFR20.M08 21:29:39.40 -40.9 54.3 85.2 98.2 9	7.7
EGFR20.M07 21:29:39.35 -43.3 58.3 85.1 98,2 9 EGFR20.M08 21:29:39.40 -40.9 54.3 85.2 98.2 9	7.7
EGFR20.M08 21:29:39.40 -40.9 54.3 85.2 98.2 9	9.7
EGFRZW. NOO ZIIZ7137140	9,7
CCEDDA MAD 31.30.30 44 -38.6 50.6 85.2 98.2 9	9.7
EGFR20, M09 21:29:39, 44 -38, 6 50, 6 65, 2 70, 2	9.7
EGFR20,M10 21:29:39.49 -36.0 46.3 85.3 98.2 9	9.7
EGFR20.M11 21:29:39.49 -36.0 46.3 85.3 98.2 9	9.7
EGFR20.M12 21:29:39.49 =36.0 46.4 85.3 98.2 9	9.7
EGFR20.M13 21:29:40.20 0.2 -12.8 86.0 98.2 9	9.7
EGFR20.M14 21:29:40.20 0.0 -12.5 86.0 98.2 9	9.7
EGFR20,M15 21:29:40.17 -0.9 -11.0 86.0 98.2 9	9.7
EGFR20, M16 21:29:40.64 22.1 -48.6 86.1 87.7 9	9,9
EGFR20.M17 21:29:40.64 22.2 -48.8 86.1 87.7 9	9.9
EGFR20, M18 21:29:40.35 8.1 -25.8 86.2 98.2 9	9.7
EGFR20.M19 21:29:40.40 10.4 -29.5 86.2 98.2 9	9.7
EGFR20.M20 21:29:40.45 13.1 -33.8 86.3 98.2 9	9.7

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg)			
FILENAME	EMIT	×	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
	****	****				
EGFR21.M01	21:33:13.24	~38,6	38.2	76.6	97.2	100.5
EGFR21.MØ2	21:33:13.24	-38.7	38.5	76.6	97,2	100.5
EGFR21.M03	21:33:13,22	-39,7	40.1	76.6	97,2	100.5
EGFR21.MØ4	21:33:13.27	=37.2	35.8	76.6	97.2	100.5
EGFR21.MØ5	21:33:13.37	-32.6	28.1	76.6	97.2	100.5
EGFR21.MØ6	21:33:13.11	-45.2	49.4	76.6	97.2	100.5
EGFR21.MØ7	21:33:13.20	-41.2	42.6	76.6	97.2	100.5
EGFR21.M08	21:33:13,28	-36.7	35.1	76.6	97.2	100.5
EGFR21.MØ9	21:33:13,36	-32,7	28.2	76.6	97.2	100.5
EGFR21.M10	21:33:13.45	-28,1	20.5	76.7	97.2	100.5
EGFR21.M11	21:33:13.45	-28.0	20.5	76,7	97.2	100.5
EGFR21.M12	21:33:13.45	-28.1	20.5	76.7	97,2	100.5
EGFR21.M13	21:33:13.88	-7.0	-15.1	76.8	97.2	100.5
EGFR21.M14	21:33:13,88	-7.1	-14.8	76.8	97,2	100.5
EGFR21.M15	21:33:13.86	-8.0	-13.4	76.8	97.2	100.5
EGFR21.M16	21:33:14,28	13.0	48.7	76.9	97.2	100.5
EGFR21.M17	21:33:14,29	13.1	-48.9	76.9	97.2	100.5
EGFR21.M18	21:33:14.25	11.1	45.6	76.9	97.2	100.5
EGFR21,M19	21:33:14.33	15.2	52.5	76.9	97.2	100.5
EGFR21.M20	21:33:14.42	19.9	-60.3	76.9	97.2	100.5

APPENDIX A

DIRECTIVITY ANGLE = 122.5 deg

FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR22, MØ1	21:36:48,78	-29.2	18.0	150.3	101.1	100.4
EGFR22, MØ2	21:36:48,77	-29.6	18.7	150.3	101.1	100.4
EGFR22.MØ3	21:36:48.74	=31.4	21.7	150.3	101.1	100.4
EGFR22.MØ4	21:36:48.69	-34.2	26,5	150.2	101.1	100.4
EGFR22, MØ5	21:36:48.71	-32.7	24.0	150.2	101.1	100.4
EGFR22, MØ6	21:36:48.45	-46.4	46.9	149.9	101.1	100.4
EGFR22.MØ7	21:36:48.51	-43,2	41.6	150.0	101.1	100.4
EGFR22.MØ8	21:36:48,59	=39.5	35,3	150.1	101.1	100,4
EGFR22.M09	21:36:48.65	-35.9	29.3	150.2	101.1	100.4
EGFR22.M10	21:36:48.65	-17.8	29.7	161.5	96.5	105.5
EGFR22.M11	21:36:48.65	-17.8	29.7	161.5	96,5	105.5
EGFR22.M12	21:36:48.65	-17.9	29.9	161.5	96.5	105.5
EGFR22.M13	21:36:49.37	1.2	-33.1	151.1	101.1	100.4
EGFR22.M14	21:36:49.37	0.9	⇒ 32.5	151.1	101.1	100.4
EGFR22.M15	21:36:49.34	-0.7	=29.8	151.1	101.1	100.4
EGFR22.M16	21:36:50.01	34.2	-88.5	151.9	101.1	100.4
EGFR22.M17	21:36:50.01	34.4	-88.7	152.0	101.1	100.4
EGFR22, M18	21:36:49.51	8,5	-45.3	151.3	101.1	100.4
EGFR22.M19	21:36:49.58	12.1	-51.3	151.4	101.1	100.4
EGFR22.M20	21:36:49.66	16.2	~ 58.3	151.5	101.1	100.4

APPENDIX A

DIRECTIVIT	Y ANGLE =	122.5 deg
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FILENAME	EMIT	x	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR23.M01	21:40:11.81	-31.4	18.4	139.9	97.3	100.9
EGFR23, MØ2	21:40:11.80	=31.7	19.1	139.9	97.3	100.9
EGFR23.M03	21:40:11.77	=33,4	21.9	139.9	97.3	100.9
EGFR23.MØ4	21:40:11.75	-34,3	23.5	139.9	97.3	100.9
EGFR23, MØ5	21:40:11.82	-30.9	17.7	139.9	97.3	100.9
EGFR23.MØ6	21:40:11.57	-43,4	39.0	139.8	97.3	100.9
EGFR23, MØ7	21:40:11.66	=39,0	31.6	139.9	97.3	100.9
EGFR23. M08	21:40:11.76	-34.1	23.1	139,9	97.3	100.9
EGFR23, MØ9	21:40:11.85	-29.4	15.1	139.9	97.3	100.9
EGFR23, M10	21:40:11.96	-24.1	6.0	140.0	97.3	100.9
EGFR23.M11	21:40:11.96	-24.1	5.9	140.0	97.3	100.9
EGFR23.M12	21:40:11.96	-24.2	6.2	140.0	97.3	100.9
EGFR23.M13	21:40:12.43	-1.3	-33.1	140.2	97,3	100.9
EGFR23.M14	21:40:12.42	-1,6	~ 32,6	140.2	97.3	100.9
EGFR23.M15	21:40:12.39	~3.1	-30.0	140.2	97.3	100.9
EGFR23.M16	21:40:13.05	29.2	-85.2	140.5	97.3	100.9
EGFR23.M17	21:40:13.05	29.3	-85.4	140.5	97.3	100.9
EGFR23,M18	21:40:12.72	13.2	-57,9	140.4	97.3	100.9
EGFR23, M19	21:40:12.82	17.9	~65,9	140.4	97.3	100.9
EGFR23.M20	21:40:12.93	23.2	-75.1	140.5	97.3	100.9

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg				
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
	****	,				
EGFR24.M01	21:43:26.70	=18.7	23.5	146.6	101,8	99.6
EGFR24.MØ2	21:43:26.69	-19,1	24.1	146.6	101.8	99.6
EGFR24.MØ3	21:43:26.65	=20.9	26.9	146.5	101.8	99.6
EGFR24.MØ4	21:43:26.58	-25,0	33.6	146.4	101.8	99.6
EGFR24.MU5	21:43:26.56	-25. 8	35.Ø.	146.4	101.8	99.6
EGFR24.MØ6	21:43:26,27	-41.3	60.1	146.0	101.8	99.6
EGFR24.MØ7	21:43:26.29	-40.1	58.2	146.1	101.8	99.6
EGFR24.MØ8	21:43:26.32	=38,4	55.5	146.1	101.8	99.6
EGFR24.MØ9	21:43:26.35	-36,8	52.8	146.1	101,8	99.6
EGFR24.M10	21:43:26.39	-34.8	49.5	146.2	101.8	99.6
EGFR24.M11	21143126.39	=34.8	49.5	146.2	101.8	99.6
EGFR24.M12	21:43:26.39	-34.9	49.8	146.2	101.8	99.6
EGFR24.M13	21:43:27.28	12.6	-27.5	147.3	101.8	99.6
EGFR24.M14	21:43:27.27	12.3	*26.9	147.3	101.8	99.6
EGFR24.M15	21:43:27.24	19.7	-24,3	147.2	101.8	99.6
EGFR24, M16	21:43:27.88	3 44.5	-79.3	148.0	101.8	99.6
EGFR24.M17	21:43:27.88	44.6	-79.5	148.0	101.8	99.6
EGFR24.M18	21:43:27.24	10.7	-24.4	147.2	101.8	99.6
EGFR24.M19	21:43:27.2	7 12.4	-27.2	147.3	101.8	99.6
EGFR24.M2Ø	21:43:27.3	1 14.5	-30.4	1.47 . 3	101.8	99.6

APPENDIX A

DIRECTIVIT	Y ANGLE =	122,5 de	g			
FILENAME	EMIT	X -	Y	Z.	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR25.MØ1	21148118.16	38,9	36.7	0 /I		****
EGFR25.MØ2		_		9.4	103,1	102.1
	21:48:18.17	38,9	36.5	9.4	103.1	102,1
EGFR25.M03	21:48:18.17	39.0	36.4	9 . 4	103.1	102.1
EGFR25, MØ4	21:48:18,31	46.2	23.5	9.4	103.1	102.1
EGFR25, MØ5	21:48:18.51	56.1	5.8	9.4	103.1	102.1
EGFR25, MØ6	21:48:18,33	46.9	22,3	9.4	103.1	102.1
EGFR25, MØ7	21:48:18.48	54.4	8.8	9.4	103.1	102.1
EGFR25, MØ8	21:48:18.64	62.5	- 5.7	9,3	193.1	102.1
EGFR25, MØ9	21:48:15.16	-108.0	291.9	9.9	57,8	90.6
EGFR25, M10	21:48:14.46	-134.2	322.5	9.6	57.8	90.6
EGFR25,M11	21:48:14.45	=134.6	322.9	9.6	57.8	90.6
EGFR25, M12	21:48:14.44	-134.9	323.3	9.6	57.8	90.6
EGFR25.M13	21:48:18.78	69,6	-18.4	9.3	103.1	102.1
EGFR25.M14	21:48:18.78	69.7	~18.6	9.3	103.1	102.1
EGFR25.M15	21:48:18.78	69,7	-18.7	9.3	103.1	102.1
EGFR25, M16	21:48:18,62	61.4	-3.7	9.3	103.1	102.1
EGFR25.M17	21:48:18.62	61.5	-4.0	9.3	103.1	102.1
EGFR25.M18	21:48:19.55	108.2	-87.6	9.1	103.1	102.1
EGFR25,M19	21:48:19.70	115.5 -	100.8	9.1	103,1	102.1
EGFR25.M20	21:48:19.86	123.8	115.6	9.1	103.1	102.1

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg				
FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)

EGFR26, MØ1	21:52:20,44	=30.2	49.4	10.4	93.3	99.7
EGFR26, MØ2	21:52:20,44	-30.2	49.4	10.4	93.3	99.7
EGFR26.M03	21:52:20.44	-30.2	49.5	10.4	93,3	99.7
EGFR26.M04	21:52:20.48	-27.9	45.6	10.4	93,3	99.7
EGFR26.MØ5	21:52:20.55	-24.7	40.5	10.5	93.3	99.7
EGFR26.MØ6	21:52:20.26	-38.9	63.6	10.4	93,3	99.7
EGFR26, M07	21:52:20,31	- 36.5	59.7	10.4	93.3	99.7
EGFR26, MØ8	21:52:20.37	-33.9	55.4	10.4	93.3	99.7
EGFR26.MØ9	21:52:20.41	-31,5	51.6	10.4	93.3	99.7
EGFR26.M10	21152120.47	-28.9	47.3	10.4	93,3	99.7
EGFR26,M11	21:52:20.47	-28.9	47.2	10.4	93.3	99.7
EGFR26.M12	21:52:20.47	-28.8	47.2	10.4	93.3	99.7
EGFR26,M13	21:52:21.12	8,5	-4.5	10.5	93.3	99.7
EGFR26.M14	21:52:21.12	2.8	-4.5	10.5	93.3	99.7
EGFR26,M15	21152:21.12	2.8	-4.4	10.5	93,3	99.7
EGFR26.M16	21152121.13	3.0	-4.8	10.5	93.3	99.7
EGFR26,M17	21:52:21.13	3.1	-5.0	10.5	93,3	99.7
EGFR26.M18	21152121.38	15.2	-24.7	10.6	93.3	99.7
EGFR26.M19	21:52:21.42	17.6	-28.6	10.6	93.3	99.7
EGFR26.M2Ø	21:52:21.48	20.2	32.9	10,6	93.3	99.7

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg				
FILENAME	EMIT	×	Y	Z	VEL	HEADING
************	TIME		(m)		(m/s)	(deg)
EGFR27, MØ1	21:55:42,94	-29.6	50.1	23.7	97,6	99.4
EGFR27.MØ2	21155:42.94	-29.6	50.2	23.7	97.6	99.4
EGFR27.MØ3	21:55:42.93	-29.8	50.5	23.7	97.6	99.4
EGFR27.MØ4	21:55:42.96	-28.2	48.0	23.7	97.6	99.4
EGFR27. M05	21:55:43.00	-26.2	44.7	23.7	97.6	99.4
EGFR27. MØ6	21:55:42.71	-41.2	68.8	23.6	97,6	99.4
EGFR27.M07	21:55:42.74	-39,5	66.2	23,6	97.6	99.4
EGFR27.M08	21:55:42.78	-37. 8	63.4	23.6	97.6	99,4
EGFR27.M09	21:55:42.81	⇒ 36,2	60.8	23.6	97,6	99.4
EGFR27.M10	21:55:42.84	-34.4	58.0	23.6	97.6	99.4
EGFR27.M11	21:55:42.84	-34.4	58.0	23.6	97.6	99.4
EGFR27.M12	21:55:42.84	=34,4	57.9	23.6	97.6	99,4
EGFR27.M13	21:55:43.59	3,7	-3,5	23.9	99.7	99.4
EGFR27.M14	21:55:43.59	3.7	-3.5	23.9	99.7	99.4
EGFR27.M15	21:55:43.58	3,5	-3.2	23.9	99.7	99.4
EGFR27,M16	21:55:43,67	8.6 -	11.3	23.9	99.7	99.4
EGFR27.M17	21:55:43.68	8.7 -	11.6	23.9	99,7	99.4

EGFR27.M18 21:55:43.73 11.7 -16.4 23.9 99.7

EGFR27.M19 21:55:43.77 13.3 =19.0 23.9 99.7 99.4

EGFR27. M20 21:55:43.80 15.1 -21.9 23.9 99.7 99.4

99.4

APPENDIX A

DIRECTIVITY	ANGLE =	122,5 deg
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FILENAME	EMIT	X	Y	Z	VEL	HEADING
	TIME		(m)		(m/s)	(deg)
EGFR28, MØ1	22:22:30.00	510.0	0.0	1,4	0,0	85.0
EGFR28, MØ2	22:22:30.00	510.0	0.0	1.4	0.0	85.0
EGFR28, M03	22:22:30.00	510.0	0.0	1.4	0.0	85.0
EGFR28.MØ4	22:22:30.00	510.0	0.0	1.4	0.0	85.0
EGFR28, MØ5	22:22:48.00	510.0	0.0	1.4	0.0	85.0
EGFR28, MØ6	22:22:48.00	510.0	0.0	1.4	0.0	85.0
EGFR28, MØ7	22:22:48,00	510.0	0.0	1.4	0.0	85.0
EGFR28, MØ8	22:22:38,00	510.0	0.0	1.4	0.0	85.0
EGFR28, MØ9	22:22:30.00	510.0	0.0	1.4	0.0	85.0
EGFR28,M10	22:22:30,00	510.0	0.0	1.4	0.0	85.0
EGFR28,M11	22:22:30.00	510.0	0.0	1.4	0.0	85.0
EGFR28, M12	22:22:30,00	510.0	0.0	1.4	0.0	85.0
EGFR28,M13	22:22:29,00	510.0	0.0	1 . 4	0,0	85.0
EGFR28 M14	22:22:29.00	510.0	0.0	1.4	0.0	85.0
EGFR28,M15	22122129,00	510.0	0.0	1.4	0.0	85.0
EGFR28.M16	22:22:29,00	510.0	0.0	1.4	0.0	85.0
EGFR28,M17	22122129,00	510.0	0.0	1 , 4	0.0	85.0
EGFR28, M18	22:22:35,00	510.0	0.0	1 . 4	0.0	85.0
EGFR28.M19	22:22:35.00	510.0	0.0	1.4	0.0	85.0
EGFR28,M20	22:22:35.00	510.0	0.0	1.4	0.0	85.0

WEATHER DATA

Average values of weather data for each run are presented herein for the following weather stations: all stations in the triangle area, the 4-m station at building C-15, the 1.2-m station at van 1, the 1.2-m station at van 5, and the 10-m station at van 3. The weather profile data is presented with the beginning and ending Greenwich mean time of each profile run.

TRIANGLE AREA WEATHER STATION

			Wind	speed	, m/se	c	Average	Tempera	ture, ^o C
Date	Run no.			Stati	on		wind direction,	Sta	tion
		3 m	6 m	9 m	12 m	15 m	deg	3 m	15 m
11/1/78	1	3.8	4.0	4.1	4.1	4.7	314	7.4	9.4
	2	3.9	4.1	4.5	4.2	4.7	316	7.0	9.4
	3	3.9	4.4	4.3	4.4	4.7	315	6.8	9.5
	4	3.6	3.8	4.3	4.1	4.8	317	6.8	9.5
	5	3.7	4.4	4.2	4.4	4.5	314	6.8	9.4
11/2/78	6	4.0	4.0	3.9	3.8	4.0	284	16.5	16.6
	7	2.8	2.7	2.9	2.9	3.0	287	16.5	16.6
	8	2.8	3.0	3.2	3.1	3.3	313	16.6	16.9
	9	2.6	2.9	2.9	2.8	2.6	284	16.9	16.8
	10	2.2	2.4	2.6	2.4	2.6	256	16.8	16.9
	11	2.4	2.6	2.9	2.8	3.2	263	16.9	16.8
	12	4.3	4.4	4.5	4.3	4.3	260	16.7	16.7
	13	4.3	4.5	4.4	4.5	4.5	282	16.5	16.4
	14	4.3	4.4	4.4	4.6	4.4	282	16.4	16.3
	15	4.1	4.2	4.1	4.4	4.3	297	16.3	16.2
	16	3.9	4.0	4.2	4.3	4.5	299	16.2	16.1
	17	4.0	3.9	4.0	4.0	3.8	303	16.1	16.0
	18	3.0	3.6	3.8	4.0	4.2	292	16.0	16.0
	19	4.2	4.3	5.0	4.7	5.2	299	15.9	15.8
	20	2.9	3.2	3.7	3.9	3.8	299	15.7	15.7
	21	3.0	3.2	3.5	3.7	3.8	289	15.6	15.6
	22	2.8	2.9	3.3	3.3	3.3	304	15.5	15.5
	23	3.4	3.6	3.4	3.9	3.8	293	15.4	15.4
	24	3.8	4.0	4.0	3.8	4.2	305	15.4	15.3
	25	2.8	3.5	3.8	4.0	3.8	295	15.2	15.2
	26	2.4	2.4	2.6	2.8	3.2	289	15.0	15.0
	27	2.2	2.4	2.5	2.4	2.6	286	15.0	15.0

BUILDING C-15 WEATHER STATION

	Τ_	Wind	Wind
Date	Run	direction,	speed,
Date	no.		
		deg	m/s
11/1/78	1	320	3.4
	2 3	320	2.7
		320	3.6
	4	315	3.1
	5	320	2.7
11/2/79	6	230	1.8
	7	250	3.6
	8	280	2.7
	9	280	2.5
	10	250	2.7
	11	245	2.7
	12	240	1.8
	13	270	3.6
	14	270	3.4
	15	300	3.6
	16	280	3.6
	17	290	2.7
	18	280	3.1
	19	285	3.6
	20	290	2.7
	21	285	2.7
	22	290	2.9
	23	290	3.1
	24	290	2.7
	25	285	2.7
	26	280	2.7
	27	275	2.2
	28	270	2.5
			l

1.2-m WEATHER STATION, VAN 1

Date	Run no.	Wind direction, deg	Wind speed, m/s	Relative humidity, percent	Temperature, OC
11/1/78	1	330	1.9	70	7.8
	2	330	1.9	70	7.8
	3	345	1.9	70	7.8
	4	345	1.9	70	7.8
	5	355	1.9	70	7.8
11/2/78	6	270	2.2	38	17.4
	7	285	2.5	38	17.9
	8	315	2.4	38	17.4
	9	315	2.4	38	17.4
	10	270	2.5	38	16.8
	11	300	2.5	38	16.8
	12	285	2.9	38	16.8
	13	290	3.1	39	16.2
	14	300	3.1	39	16.2
	15	315	3.4	40	15.7
	16	315	3.4	40	15.7
	17	315	3.5	40	15.7
	18	315	3.6	40	15.7
	19	315	3.6	40	15.7
	20	310	2.2	40	15.1
	21	310	2.2	40	15.1
	22	315	2.2	40	15.1
	23	315	2.2	40	14.6
	24	315	2.2	40	14.3
	25	320	2.2	40	13.4
	26	300	1.9	40	13.4
	27	300	1.9	40	13.4
	28	295	1.4	42	11.2

1.2-m WEATHER STATION, VAN 5

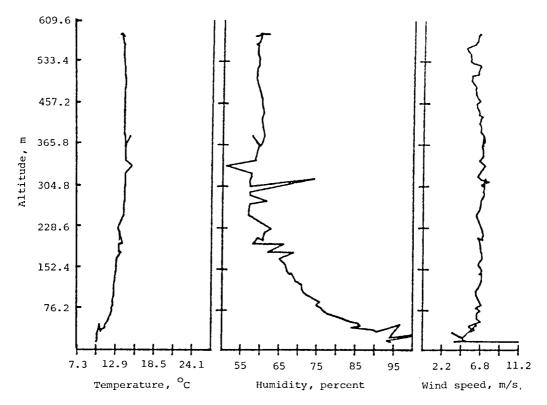
Date	Run no.	Wind direction, deg	Wind speed, m/s	Relative humidity, percent	Temperature, OC
11/1/78	1	320	3.2	97	6.2
	2	325	3.2	96	6.7
•	3	325	3.2	96	6.7
	4	330	2.7	96	6.7
	5 6	330	2.7	96	6.7
11/2/78	6	270	2.5	82	16.8
	7	290	2.5	82	16.2
	8	270	2.5	82	16.2
	9	240	2.5	82	15.7
	10	240	2.5	82 `	15.7
	11	250	2.5	82	15.7
	12	260	2.5	82	15.7
	13	270	2.7	82	14.6
	14	280	2.7	82	14.6
	15	285	2.5	82	14.0
	16	285	2.5	82	13.4
	17	285	2.3	82	13.4
	18	275	2.3	82	13.4
	19	275	2.3	82	13.4
	20	270	2.3	82	13.4
1	21	300	1.4	82	13.4
1	22	285	1.4	82	13.4
	23	255	1.4	82	12.9
1	24	265	1.4	82	12.3
	25	270	1.4	82	11.8
	26	255	1.4	82	11.2
	27	255	1.4	82	11.2
	28	255	1.3	82	10.1

10-m WEATHER STATION, VAN 3

Date	Run no.	Wind direction, deg	Wind speed, m/s	Barometric pressure, kPa	Temperature, oC	Relative humidity, percent
11/1/79	1	19.0	3.2	101.62	8.3	100.0
	2	25.0	2.7	101.62	8.3	99.0
	3	23.0	3.6	101.62	8.9	98.0
	4	31.0	3.6	101.62	9.4	95.0
	5	22.0	2.7	101.62	9.4	95.0
11/2/79	6	330.0	3.2	101.62	17.8	35.0
	7	344.0	1.4	101.90	17.8	35.0
	8	354.0	2.2	101.90	17.2	35.0
	9	4.0	1.4	101.90	17.2	35.0
	10	333.0	3.2	101.90	17.2	34.0
	11	359.0	1.8	101.90	17.2	34.0
ļ .	12	340.0	2.2	101.62	17.2	34.0
	13	342.0	2.7	101.79	16.7	36.0
	14	335.0	2.7	101.83	16.7	36.0
	15	360.0	2.7	101.83	16.1	37.0
	16	358.0	2.7	101.83	16.1	37.0
	17	356.0	2.2	101.83	16.1	38.0
	18	2.0	2.7	101.83	16.1	38.0
	19	6.0	2.7	101.79	15.6	39.0
	20	6.0	2.7	101.79	15.6	39.0
•	21	2.0	2.2	101.83	15.6	39.0
	22	6.0	2.7	101.83	15.6	39.0
	23	2.0	2.2	101.79	15.6	39.0
	24	6.0	1.8	101.83	15.6	39.0
	25	6.0	2.2	101.79	15.0	39.0
	26	4.0	1.8	101.79	15.0	39.0
	27	359.0	1.4	101.79	14.4	39.0
	28	349.0	1.4	101.76	13.3	42.0

N-159 WEATHER STATION

Date	Run no.	Barometric pressure, kPa	Wind speed, m/s	Wind direction, deg	Temperature, OC	Dewpoint, OC
11/1/78	1	101.9	2.2	325	9.0	6.0
	2	102.1	2.2	325	9.0	6.1
	3	102.2	2.2	325	9.0	6.2
	4	102.2	2.2	325	9.5	6.2
	5	102.2	2.2	325	9.5	6.2
11/2/78	6	102.0	1.8	340	18.5	-15.5
}	7	101.9	2.2	330	18.5	-15.4
	8	101.9	1.8	340	18.5	-15.2
	9	101.9	2.7	345	18.5	-15.7
!	10	101.9	1.8	340	18.2	-15.1
	11	101.9	4.0	15	18.2	-15.1
•	12	101.9	2.2	0	18.2	-15.1
	13	101.9	2.2	350	17.6	-15.0
	14	101.9	2.2	340	17.6	-15.1
	15	101.9	2.2	345	17.4	-15.1
	16	101.9	2.2	335	17.4	-15.1
	17	101.9	1.8	330	16.8	-15.1
	18	101.9	2.2	340	16.8	-15.1
	19	101.9	2.7	340	16.5	-15.1
	20	101.9	3.6	320	16.5	-15.2
	21	101.9	2.7	340	16.2	-15.2
	22	101.9	1.4	5	16.2	-15.2
	23	101.9	1.8	340	16.0	-15.3
	24	101.9	1.8	335	16.0	-15.4
	25	101.9	.9	350	15.7	-15.5
	26	101.9	.9	5	15.7	-15.5
	27	101.9	1.4	350	15.4	-15.6
	28	101.9	1.8	345	15.4	-15.6
	29	101.9	1.4	350	14.3	-16.0



Date - 11/1/78; Ascent - #1; G.m.t. - Start - 11:45, End - 12:04

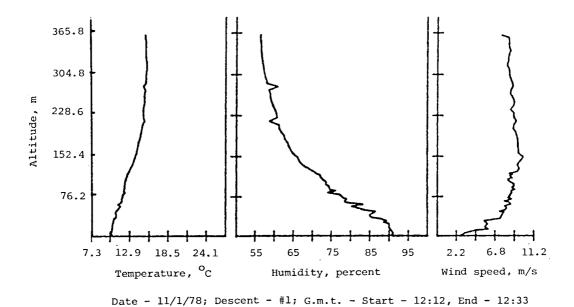
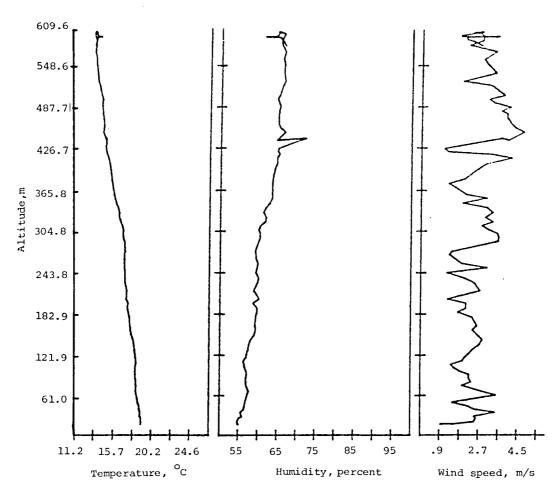
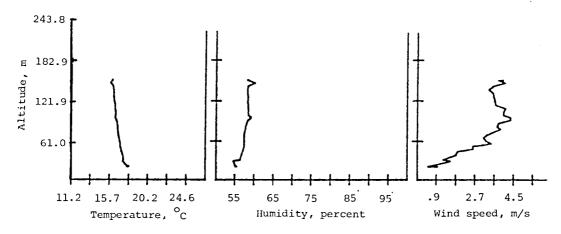


Figure Bl.- Profiles obtained by balloon station.

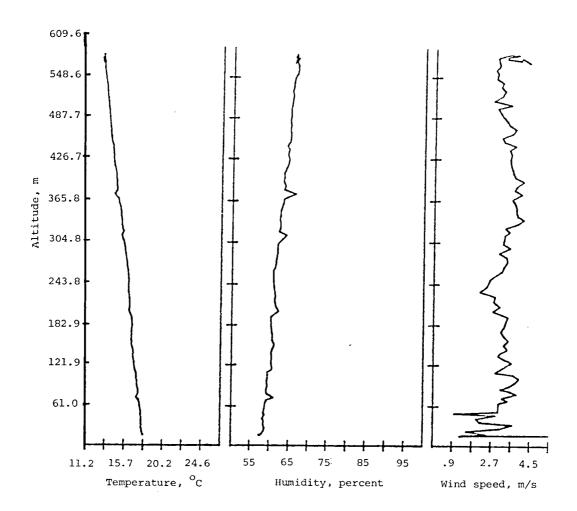


Date - 11/2/78; Ascent - #1 G.M.T. - Start - 19:06, End - 19:33



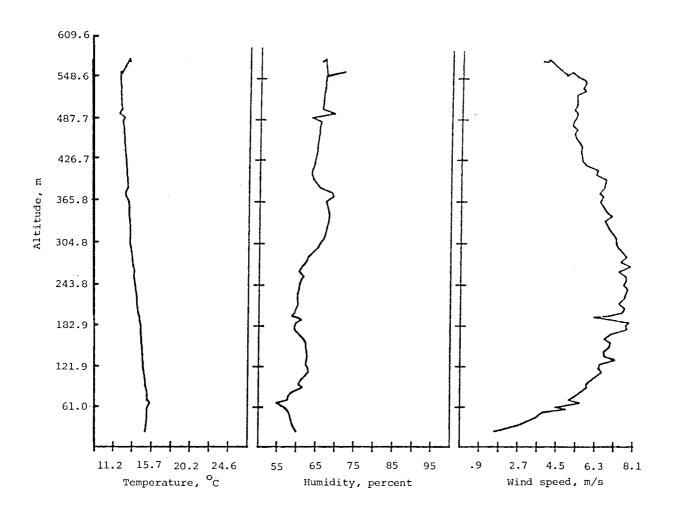
Date - 11/2/78; Descent - #1; G.m.t. - Start - 20:19, End - 20:23

Figure Bl.- Continued.



Date - 11/2/78; Ascent - #2; G.m.t. - Start-20:41, End-20:58

Figure Bl.- Continued.



Date - 11/2/78; Descent - #2; G.m.t. - Start-21:36, End-21:50

Figure B1.- Concluded.

APPENDIX C

ACOUSTIC DATA

A 1/3-octave spectrum is tabulated in this section for each microphone for each run. The spectra listed are averages of the two 1/3-octave band spectra located on either side of the reception time, calculated using the 122.5° directivity angle criteria. The 1/3-octave bands from 10 Hz to 2 kHz are included along with the reception time, the elevation angle β , and the slant range of the overall sound pressure level (OSPL) associated with each spectrum. The data for a particular run and microphone are identified with the following nomenclature EGFR ##.M**, where ## is the run number and ** is the microphone number.

DIRECTIVITY ANGLE = 122.5 deg

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	3.16	0.20	0.25	0.32	0.40	0.50	0,63	0.79	1.0	1.3	1.6	2.0	
	TIME	(deg)	(m)																
EGFRØ1.MØ1	11:46:38,69	3.2	212.9	100.4	76.9	82.4	87.6	91.7	94.2	93.5	94.2	91.8	85.2	79.9	78.0	76.5	76.8	74.6	
	11:46:38,70	2.8	215.9	• •								89.3			-	-	-	_	
EGFR01, M03	11146138,71	Ø.7	218,6	102.4	75.0	84.2	88.8	94.0	95.2	88.6	88.4	95.1	88.7	91.3	90.7	90.1	88.7	85.4	
EGFRØ1, MØ4	11:46:39,38	1.4	434.0	89.2	70.6	68.4	68.5	68.3	6A.A	69.9	76.4	79.9	80.5	81.8	81.4	80.2	74.9	75.1	
EGFRØ1.MØ5	11:46:40,30	0.8	729.1	85.5	76,2	73.2	71.3	64.6	66.6	66.7	74.1	74.5	77.0	74.8	72,6	68.9	67.6	64.7	
EGFRØ1, MØ6	11:46:40,46	0.7	885.1	86.0	65.7	64.4	64.4	68,5	68.2	70.0	71.6	74.8	75.9	78.9	79.2	75.3	71.5	70.6	
EGFRØ1.MØ7	11146141.16	0,6	1110.7	88,0	73.2	80.0	80.6	78.1	69.7	65.8	74.6	78.5	77.9	78.5	71.4	72.7	70.6	68.9	
EGFRØ1, MØ8	11:46:41.92	0.5	1352.3	82.3	65.4	68,1	68.4	66.8	62.1	69.2	70.2	74,9	76.0	72.9	70.6	66.3	64.5	63.3	
EGFRØ1.MØ9	11:46:42.61	0.4	1572.2	84.6	64.3	64.9	70.3	66.1	61.7	66.0	73.6	76.4	80.5	77.0	73.0	69.5	65.8	63,0	
EGFRØ1.M1Ø	11:46:43.38	0.4	1816.5	79.3	68,6	62,2	67.6	63,5	65.6	73.2	72,0	69.1	67.1	64.5	60,8	57.1	55.6	53.0	
EGFRØ1,M11	11146143.38	0.3	1819.6	77.3	65.6	56.5	62.0	59.4	58.0	63.5	67.1	68,8	70.3	70.4	65,3	60.2	58,2	56.0	
EGFRØ1,M12	11146143.39	0,1	1855.6	84.0	65,2	60.4	64.6	67.9	70.5	74.6	75.6	76,2	74.1	75.0	73.3	71.8	67.6	62,1	
EGFRØ1.M18	11146143.11	0.4	1401.6	86.3	68.0	62,0	72.4	74.0	82.0	77.5	74.1	68.5	68,7	71.2	68.8	69.2	66.6	65.4	
EGFRØ1, M19	11:46:43.80	0.4	1621,5	82,3	66,6	67.7	72.3	71.4	75.>	72.1	66.6	66.3	66.8	71.1	68,5	66,8	64,5	61.8	
EGFRØ1.M2Ø	11:46:44,58	0.3	1868.9	81.8	63.4	60.7	70.6	71.4	76.1	74.8	68,1	68.3	67.4	67.5	66.1	64.9	60,3	56.3	

FILENAME	RECEIVE	BETA	SR	OSPL	0,10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
***********	TIME	(deg)	(m)															
EGFRØ2.MØ1	11154128,21	3.1	216.7	99.4	79.0	77.8				-			84.3					73.9
EGFRØ2.MØ2	11:54:28,21	8,5	219.7	98.3	79.4	81.4	80.5	82.1	89.9	89.1	90.7	89.3	88.7	87.7	84.6	84.1	85.9	84.6
EGFRØZ, MØ3	11:54:28.22	0.7	222.4	103,2	75.2	77.9	88.5	92.9	95.5	90.8	90.8	97.5	90.9	93.4	90.4	91.9	89.7	86.7
EGFR02.M04	11:54:28,90	1.4	437.8	93,3	80.8	77.4	71.8	73.4	70.3	73.6	80.4	81.8	81.0	82.2	85.2	79.9	78.2	79.0
EGFRØ2.MØ5	11:54:29.82	0.8	732.9	87.5	74.5	79.5	73.8	73.0	69.1	69.7	72.1	75.0	78.5	81.1	76.3	75.1	70.6	71.3
EGFRØ2.MØ6	11154129.97	0.7	888.9	85.1	70.7	67.3	64.4	65.8	70.2	69.8	70.6	73.1	79.4	77.0	75.2	70.7	70.4	69.6
EGFRØ2.MØ7	11:54:30.67	0.5	1114.5	89.0	78,6	79.5	79.5	72,5	65.9	66.4	74.4	77.2	77.6	80.1	79.6	75.7	75.0	70,9
EGFRØ2, MØ8	11:54:31.43	3,4	1356.1	84.0	65.6	65.1	66.6	64,4	66.7	68.8	73.2	76.6	81.1	76.4	71.9	69,5	67.4	66.0
EGFRØ2.MØ9	11:54:32.12	0.4	1575.9	82.9	64.1	68.0	67.7	64.3	63.4	66.9	70.6	73.0	70.9	69.4	68.7	68.1	64.5	62.0
EGFR02.M10	11:54:32.89	0.4	1820,3	76.5	60,4	66.2	62.0	66.6	68.1	66,3	65.6	59,9	61.1	62.5	59.4	60.6	59.5	54,4
EGFRØ2, M11	11154132.90	0.3	1823.4	75.8	60,3	58.6	60.8	59.7	62.A	59.9	63.2	64.4	66.9	68.9	63.0	62.3	60.7	56.6
EGFRØ2,M12	11454132.91	0.1	1826.4	87.3	65.3	65.8	66.0	70.3	73.2	69.1	75.1	66.5	67.9	66.8	66.8	63,5	61.8	59,1
EGFR02, M13	11154129.02	2.7	249.8	97.5	78.4	74.2	77.3	81.4	89.A	91.2	89.0	84.0	86.2	86.8	87.2	83.9	82.6	80,9
EGFRØ2.M14	11:54:29.03	2.4	252.8	100.2	82.4	89.1	91.0	92,3	93.4	92.0	91.3	87.4	84.4	80.1	74.8	80.6	79.9	79,0
EGFRØ2.M15	11154129.03	0.6	255.6	105.4	81.0	84.5	91.2	94.8	96.1	98.5	96.5	94.1	92.6	94.0	91.1	89.0	90,4	90.5
EGFRØ2.M16	11154128.33	54.8	13.1	100.6	90.3	91.2	91.4	89.7	89.5	90.5	87.7	86,9	87.5	82.0	83.3	83.8	84.4	81.8
EGFRØ2.M17	11154128,33	54.5	13.1	111.3	100.5	101.0	103.1	99.7	94.9	96.2	101.2	105.2	102.9	98,2	96.1	98.7	98.3	97.2
EGFRØ2.M18	11154132.64	0.4	1405.4	91.6	73.0	76.8	81.5	84.3	86.0	86.1	76.3	73.3	76.0	72.3	71.2	70.9	66.4	61.6
EGFRØ2. M19	11154133,33	0.4	1625.3	84.3	70.4	67.8	68,0	74.6	74.3	72.7	69.2	70.2	77.1	74.0	72.0	67.5	63.2	61.1
EGFR02.M20	11:54:34.10	0,3	1872.7	82.3	68.3	67.8	62.1	66.4	75.2	74.9	75.0	70.2	67.2	68,2	67.2	64.3	60,1	57.3

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0,50	0,63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFRØ3.MØ1	11:58:55.15	3.2	214.2	100.6	78.6	77.2	85.2	91.0	_	-			AT A				74.7	7/1 0
	11:58:55.16	2.8	217.2														_	-
_	• •	- •															62.8	
-	11:58:55,16	0.7	219.9	105.9	78.1	83.1	85,9	94.1	96.1	87.0	93.8	95.7	88,8	93.2	92,9	91.2	91.4	88.6
EGFRØ3.MØ4	11158155,85	1 . 4	435.7	91.5	75.1	68.6	66,8	- 69,3	70.1	72.1	86.9	81.0	81.8	79.9	85.1	81.0	78.9	79.3
EGF903.M05	11158156,79	0.8	731.4	81.6	62.9	67.6	70.6	70.2	71.2	67.5	69,8	70.6	68.6	69.8	71.9	70.3	71.2	64.8
EGFRØ3.MØ6	11:58:56.95	0.7	887.8	87.2	71.1	72.1	69,9	67.5	68.6	72.3	77.3	75.6	78.3	79.9	78.0	73.7	71.7	70.6
EGFRØ3.MØ7	11158157,66	Ø.6	1113.9	87.5	75.1	75.4	72.5	63,3	67.A	72.6	75.9	76.2	77.6	79.5	76.8	75.0	72.5	70,9
EGFRØ3, MØ8	11158158,43	0.5	1355.9	86.7	65,1	65.2	66,8	62.5	66.A	68.0	76,5	81.7	81.0	76.7	76.3	68.3	69.3	68,4
EGFRØ3, MØ9	11158159,13	0.4	1576.2	86.8	68,5	67.2	64.8	59.4	60.A	66.5	70.3	69.4	68.3	71.2	72.1	66.2	64.1	62,5
EGFR03.M10	11158159.91	0.4	1821.0	81.9	66,4	65.7	67.9	64.6	65.7	69.5	67.3	67.7	66.1	62.4	61.3	58.3	58.8	58.2
EGFRØ3.M11	11158159.91	0.3	1824.1	78.9	62.7	63.6	61.7	57.5	60.A	62.7	64,9	68.1	68.3	67.5	65.4	63.0	62.3	58.3
EGFR03,M12	11:58:59,93	0 . i	1827.1	85.4	66.3	67.1	67,1	72,0	75.1	75.4	72.8	69.9	70.7	69.4	70.0	67.0	65,0	62,5
EGFR03, M13	11:58:55,95	2.8	247.2=	1520.9	60.9	821.0	485.1	-444.0	313.9-	108.1	399.1	-21.7	147.1	145.8	62.2	820.2	483.3	-24.1
EGFRØ3.M14	11158155.96	2.4	250.2	-91.4	-27.1-	110.7	57.2	476.7-	700.5-	448.9	309.9	58.3	563.8	229.2	277.6	900.5-	530.5	307.8
EGFRØ3.M15	11:58:55.97	0.6	253.0	160.5	62.7	229.8	-526.7	398.6	189.4	316.0	401.6	401.3	990.7	653.5	-20.1	821.8=	-189.1-	107.9
EGFRØ3, M16	11:58:55.28	57.5	12.7	686.1	166.1	251.7	166.9	688,6	-91.0-	347.0	166.0	80.4	167.1	-5.9	-5.7	81.0	165.8	-5.8
EGFR03, M17	11:58:55.28	57.4	12.7	-251.5	-86.6	-86.1	84.0	770.5-	257.4-	257.9	-0.4-	428.7	-0.5	84.7	-86,9	85.4	-86,1-	173.0
EGF903.M18	11158159,63	0.4	1405.0	84.3	70.6	70.8	65.3	72.5	75.4	72.1	71.0	69.0	70.5	71.8	67.0	71.3	68.4	65,1
EGFRØ3.M19	111591 0.32	0.4	1625.5	83.4	69.0	70.7	71.3	72.4	76.a	70.7	66.5	69.1	68.0	68,4	70.0	72.3	68.7	64.0
EGFRØ3, M2Ø	111591 1.11	0.3	1873.6	80.6	67.9	69.7	71.9	69.6	72.0	72.1	68,2	66.6	66.1	63.4	62.9	63,9	62,3	59,4

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	8.48	8.50	R, 63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGPRØ5.401	121 6159,82	3.2	220.3	100.1	79.5	80.8	84.7	85.8	91.9	96.1	94.2	89.7	84.3	79.1	75.3	74.3	75.6	73.1
EGFR05. M02	12: 6:59.83	2.9	223.2	99.5	80.0	80.8	83.7	83.4	90.4	91.9	93.4	91.2	89,9	85.9	84.6	83.8	83.8	82,3
EGFRØ5. MØ3	121 6159,84	8.6	225.9	103.3	74.2	85.8	90.8	90.5	95.4	91.8	93.2	97.3	90.7	93.6	91.0	92.6	89.5	84.6
EGFR05, M04	12: 7: 0,50	1.5	440.8	92.5	73.4	70.0	65,3	66.4	68.4	73.9	80.7	80.8	82,1	82.1	85.0	85.6	82.1	75.6
EGFRØ5.MØ5	12: 7: 1.40	0.9	735.1	83.0	70.2	70.3	70.3	70.3	70.A	69.8	70.0	73.1	72,4	74.5	75.4	71.7	69.7	68.9
EGFRØ5, MØ6	12: 7: 1.55	0.7	892.6	88,8	66,2	70.4	72.8	70.4	73.9	76.8	82,2	79.7	78.1	82.0	79.7	78.8	76.9	71,6
EGFRØ5.MØ7	12: 7: 2.24	0.6	1115.7				79.0											
EGFRØ5.MØ8	12: 7: 2.98	0.5	1356.6				67.1											
EGFR05, M09	12: 7: 3.66	0.4	1575.9				70.0											
EGFRØ5. M10	12: 7: 4.41	0.4	1819.7				66.4											
EGFR05. M11	12: 7: 4.41	0.4	1822.7				59.6											
EGFRØ5, M12	12: 7: 4.43	0.1	1825.8				68.6											
EGFR05, M13	12: 7: 0.61	2.8	253.6				84.2											
EGFRØ5.M14	12: 7: 0.62	2.5	256.6				89,8											
EGFR05, M15	121 71 0,62	0.7	259.3				95.2											
EGFR05.M16	121 6159,91	47.0	15.4				100.0											
EGFRØ5.M17	121 6159,92	46.6	15.5				88.8											
EGFRØ5.M18	12: 7: 4.15	0.5	1406.3				81.7											
EGFRØS.M19	12: 7: 4,82	0.4	1625.6				80.3											
	121 71 5,59		1872.4															
TOLINDS INCO	181 18 3834	6.2	10/6.4	14.2	00.0	/1.0	72.1	66.2	68.0	70.1	64.3	65.7	63,4	64.7	61.3	61.0	56.9	56.3

1/2	OCTAVE	RAND	CENTED	FREQUENCIES	(kHz1
1/4	III. TAVP	M A NII	LENIER	PREMILENLIES	LETZI

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFRØ6, MØ1	19:37:36,44	3.4	219,6	93,6	80.5											67.8		
EGFRØ6, MØ2	19137138,45	3.1	222.6	93.6	80.6	84.9	82.5	82.0	84.5	84.5	84.3	83.8	80.0	79.3	77.9	74.3	74.4	69.3
EGFRØ6.MØ3	19:37:38,45	1.0	225.2	103.1	75.6	76.5	82.1	87.3	94.3	96.4	98.0	94.6	87.5	90.7	85.6	87.2	86.8	85.1
EGFRØ6.MØ4	19137139,09	1.6	439.4	86.4	75.1	76.4	77.3	71.2	72.5	69.9	70.8	76.5	74.9	76.8	76.7	70.2	67.2	65.1
EGFRØ6.MØ5	19:37:39.98	0.9	732.9	72.3	61.3	61.5	61.9	55.7	52.7	51.6	55.2	53,5	56.8	56,2	54.2	54.9	54.2	50.3
EGFRØ6, MØ6	19:37:40.11	0.8	887.7	74.0	59.5	63.4	54.4	58.5	53.0	53.0	55.1	53.1	53.3	55,6	54.9	54.6	52,5	48.5
EGFRØ6.MØ7	19:37:40.78	0.6	1112.1	68.5	60.1	61.8	55.4	50.1	52.3	50.8	51.0	52.6	56.4	54.8	53.4	52.0	51.1	47.2
EGFRØ6.MØ8	19:37:41,51	0.5	1352.3	66.4	59.8	53.2	58.0	51,9	53.7	53.0	51.5	52.4	52.1	55.6	54.2	54.5	50.3	49.6
EGFRØ6, MØ9	19:37:42.17	0.4	1571.0	65,8	55.0	54.9	55.5	52.4	51.2	49.5	50.5	51.6	52.4	51.8	51.7	59.9	49.3	48.4
EGFR06.M10	19137142.84	0.5	1835.6	63.9	49.4	50.3	55.5	49,6	52.3	48.6	49.1	48.5	47.2	45.8	45.4	45.6	43.2	42.5
EGFRØ6.M11	19:37:42.86	ð.5	1838.6	61.2	47.3	47.7	54.5	49,9	48.2	45.5	46.0	49.6	52.2	50.3	49.3	47.4	44.5	42,5
EGFRØ6, M12	19:37:42.87	0.2	1841.6	68.1	47.1	49.3	58.6	52.2	52.0	57.6	56.7	55.5	51.8	52.9	50.8	51.2	45.8	43.2
EGFRØ6.M13	19:37:39.23	3.0	253.2	98.9	80.0	83.9	87.7	87.9	82.4	78.4	85.3	92.7	92.6	88.3	87,5	87.1	85.2	78.3
EGFRØ6.M14	19:37:39.23	2.7	256.2	99.1	76.6	82.1	80.6	80.3	77.9	76.5	78.3	73.6	71.3	67.3	67.9	69.2	67.9	65,3
EGFRØ6.M15	19137139.24	0.9	258.9	96.7	80.2	80.8	83.6	88.4	86.7	87.7	87,3	86.4	85.3	84.4	85.6	78.6	76.4	72.4
EGFRØ6.M16	19:37:38.55	47.4	16.3	123.1	102.3	102.9	99,8	102.8	110.1	114.2	112.5	113.7	113.1	115,3	111.6	111.1	108.7	105.6
EGF906. M17	19137138.56	47.1	16.4	123.0	102.0	102.0	120.5	102.1	110.9	113.9	112.7	115.4	113.3	115.7	111.8	111.0	108.6	107.1
EGFRØ6.M18	19137142,69	0.5	1402.4	70.3	53.1	52.6	53.1	52,5	54.1	57.1	56.2	55.5	55.3	53.1	51.5	49.6	49.1	47,3
EGFRØ6.M19	19:37:43.35	0 4	1621.0	65.3	54.6	50.8	57.1	56,6	53.5	54.6	54.1	52.1	53.1	52.0	50,9	49.0	48.3	47.2
EGFRØ6.M2Ø	19:37:44.09	P.4	1867.1	64.4	50.0	47.8	57.9	51.2	54.2	53.3	50.4	51.5	48.4	47.2	46.4	44.7	43.1	42.3

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	Ø.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
,	TIME	(deg)	(m)															
FGFPa7.Mai	19142148,59	1.8	215.1	01.5	82.2	85.4	88.5	A4.1	80.7	70.4	79.2	75.5	71.1	65,6	62 1	60.7	60 3	59.4
		•																
•	19:42:48.59	1.5	218.1	• •	-		•	-		-	-	-	-	70.5	•	•	•	_
EGFRØ7.MØ3	19:42:48.60	-2,6	1.155	184.8	-		-						-				•	-
EGF907. M04	19:42:49,27	0.7	435.9	83.8	74.9	79.2	77.7	69.3	64.1	59.1	59.3	57.1	62.7	61.4	59.7	60.8	58.9	57.6
EGFRØ7. MØ5	19:42:50.17	0.4	730.4	72.7	63,1	67.7	61.6	54.1	51.4	52.3	53.7	57,0	58.8	59.1	59.1	56.7	54.9	51.4
EGFR07. M06	19:42:50.32	0.4	886.0	71.6	64.7	65.0	60.2	52.5	53.4	53.7	54.6	54.8	56.7	58.4	56.0	56.5	54.6	51,5
EGFRØ7.MØ7	19:42:51.02	2.3	1111.2	70.9	60.3	63.9	55,9	53.0	54.3	52.5	54.1	53.2	57.5	55.7	54.6	54.0	51.7	47.5
EGFRØ7. MØ8	19:42:51.76	0.2	1352.2	67.7	58,2	50.5	48,3	48.7	46.1	47.9	50.7	55.4	56.9	57.6	58,5	56.5	52.2	49.9
EGFR07. M09	19:42:52.44	3.2	1571.6	68,8	58.2	52.3	53,8	49.6	49.5	52.1	53.5	55.1	54.2	55.8	54.2	52.0	50.8	45,9
EGFR07. M10	19142153,19	0.2	1815.5	76.8	55.6	53.2	53.4	51.8	49.3	56.1	55.4	52.4	50.1	48.7	48.0	46.4	43.9	40.0
EGFRØ7.M11	19:42:53.20	0.2	1818.6	67,6	51.1	47.6	44.7	48.9	46.4	50.0	51.3	52.4	56.1	56,5	54.6	52,9	49.8	45.4
EGFR07.M12	19:42:53.20	-3.1	1821.6	79.1	51.2	49.1	54.8	58.1	56.9	61.4	63.0	60.4	59.5	55,2	54.3	53.4	50.2	45.6
EGFRØ7.M13	19:42:49.36	1.6	248.4	100.9	79.1	86.8	89,4	87.5	90.1	92.8	94.1	94.4	89.1	84.4	87.0	89.2	85.8	80.7
EGFR07. M14	19:42:49.38	1.3	251.5	91,9	77.8	80.8	82.9	81.7	82.5	80.3	81.0	80.5	79,6	71.5	79.1	66.4	65.4	64.0
EGFRØ7.M15	19:42:49,38	-0.5	254.5	95,2	82.9	83.9	83.8	82.6	84.9	90.0	88.7	84.6	78.2	77.4	78.7	76.5	71.2	68.1
EGFRØ7.M16	19:43: 9.34	***	1930.2	89,0	80.2	81.0	81.0	82.1	80.4	81.8	81.4	80.6	81.0	81.1	80.0	81.4	80.6	79.5
EGFR07. M17	19:43: 9.34	***	1929.9	94.4	84.9	85.1	85.2	87.4	85.4	86.0	85.5	85.9	86.3	84.8	84.4	86.2	85.4	84.9
EGF907. M18	19:42:52.91	ø.2	1401.8	70.8	59,9	65.8	59.0	58.6	61.7	60.4	58.5	57.9	56.5	55,9	52.7	53,1	50,6	45.4
EGFRØ7.M19	19142153,59	0.2	1621.2	69.4	58.3	56.2	50.8	53.3	58.3	59.7	57.1	55.5	53.3	53,1	51.6	50.6	47.4	46,2
EGFRØ7.M2Ø	19142154.36	0.2	1868.1	73.5	58.4	60.0	55,4	48.3	54.0	56.5	60.8	58.8	58.4	55.8	54.6	52.5	50.1	45.2

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFRØ8.MØ1	19148146.42	2.2	213.9	94.7	81.4												69.5	65,2
EGFRØ8. MØ2	19:48:46.44	1.9	216.9	96.6	82,0	80.5	75.2	80.8	84.4	84.0	85.8	87.1	86.1	85.8	86.2	86.3	86.0	85.0
EGFRØ8, MØ3	19:48:46.44	-0.2	219.8	100.3	82.0	81.4	75.5	85.9	89.6	95.1	95.1	92.5	83.0	86.7	84.3	84.1	83.0	78.8
EGFRØ8.MØ4	19148147.11	2.9	434.8	83.5	76.1	77.0	70.8	70.1	64.5	60.7	62.9	67.1	66.7	61,3	62,8	61.4	58.8	58.7
EGFRØ8.MØ5	19:48:48.22	0.6	729,6	80.6	52.7	58.9	58.5	55.6	47.0	50.4	53,3	57.0	59.8	59.6	59.5	54.6	55.1	51.8
EGFRØ8, MØ6	19:48:48.18	0.5	885.3	77.6	56.4	60.0	57.0	54.5	54.0	54.3	56.4	56.1	62.3	63.4	63.6	61.6	59.2	56.7
EGFRØ8.MA7	19:48:48.88	0.4	1110.7	70.9	59.7	67.0	60.9	56.0	50.0	51.0	53,5	54.2	56,8	55.0	56,9	56.8	54.3	49.7
EGFRØ8.MØ8	19148149.63	0.3	1352.0	67.6	53,2	53.6	51.2	49.9	53.5	51.5	53.9	57.9	57.0	59.0	54.9	50.5	51.7	47.6
EGFRØ8, M09	19:48:50.30	0.3	1571.6	71.0	56,5	56.7	52.7	50.9	50.4	50.0	55.5	52.1	54,8	59.6	56.2	55.7	50.3	46.5
EGFRØ8.M1Ø	19:48:51.06	0.3	1815.7	63.5	47.7	48.5	46.7	47.0	44.1	47.4	47.5	47.8	44.6	41.8	40.8	39.3	36.4	33,5
EGFRØ8.M11	19:48:51.07	0.2	1818.8	59.7	44,9	41.6	45.4	40.4	41.5	43.3	48.0	48.7	49.3	48.9	46.8	44.8	43.6	40.1
EGF908, M12	19:48:51.08	-0.0	1821.8	73.5	55.6	53.8	51.3	55,3	60.0	65.7	67.0	62.2	62,0	61.7	56.5	53.8	49.4	46.5
EGFRØ8, M13	19:48:47.22	1.9	247.1	99.6	.77.4	81.7	85.3	87.6	88.8	88.8	86.6	83.2	89.3	93.5	90.5	85.7	89.4	83,6
EGFR08.M14	19:48:47.22	1.6	250.1	92.8	79,6	77.6	78.6	77.1	77.4	78.6	80,1	82.2	82.5	77.9	76.8	74.9	74.1	72.0
EGFR08, M15	19:48:47.21	-0.2	253.1	94.1	85,6	84.1	85.2	84.3	84.4	87.3	84.3	83.5	78.3	77.5	72.7	72.5	71.0	67,6
EGFRØ8.M16	19148146.49	56,8	8.5	121.9	102.1	99.4	98.8	98.0	102.0	110.2	115.6	117.9	114.0	104.8	195.6	104.3	106.8	108.0
EGFRØ8.M17	19:48:46.49	56.5	8.6	121.8	103.2	101.1	99,7	98,1	195.2	110.7	115.4	118.1	112.0	105.9	105.6	104.4	106.4	107.2
EGFRØ8, M18	19:48:50.77	0.3	1401.5	72.8	60.0	63.1	57.1	59.3	62.1	66.1	63.2	58.5	56.2	57.8	53.7	49.3	47.0	43.8
EGFRØ8.M19	19:48:51.45	0.3	1621.1	66,9	54.1	55.8	52.8	55.4	55.2	59.5	56.1	54.8	53.5	52.2	50.8	48.9	44.7	40.9
EGFRØ8,M2Ø	19148152,22	2.2	1868.2	67.9	51.5	57.3	52.0	50.7	53.0	54.0	53.4	51.3	52.3	51.1	47.1	45.6	42.1	39,4

FILENAME	RECEIVE	BETA	SP	OSPL	0.10	2.13	0.16	a.2a	0,25	0.32	0.40	2.50	0.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
FGFRA9. MA1	19:52:39.03	1.5	214.9	011 6	82 A	84 5	82 1	AD 0	81.4	_						44 0	6/1 T	41 7
•	•	-		•	-	-		•				-	•		-	•	•	- •
	19:52:39.04	1.2	217,9	•	•		-	-	81.2	-		-		-		-	•	•
EGFRØ9.MØ3	19152139.05	-0.9	220.9	101.0	83.9	82.4	82.5	80.6	88.0	91.9	94.9	96.1	90.7	85.4	82,9	86.8	87,7	83,1
EGFRØ9, MØ4	19152139.72	0.6	436.1	82.9	75.6	74.9	74.6	72,3	64.5	59.8	59.3	64.3	65.2	64.6	65.6	65.2	59.7	61.2
EGFR09. M05	19:52:40.64	0.4	731.3	74.1	64.6	60.6	54.4	51.3	49.1	49.6	58.4	55.5	56,4	61.5	57.8	57.0	54.4	50.3
EGFRØ9, M06	19:52:40.80	0.3	887.3	74.4	65.0	65.9	56.9	51.3	52.5	50.5	54.9	56.5	57.6	58.3	57.5	55.2	52,4	49.7
EGFRØ9.MØ7	19152141.51	0.2	1113.0	76.7	57.4	64.2	50.5	56,4	53.7	53.8	56.4	55.3	53,5	54.9	52,4	52.3	50.4	47.4
EGFRØ9.MØ8	19:52:42.26	0.2	1354.5	69.6	53,8	47.4	44.7	48.0	49.4	48.2	49.8	54.6	53.7	52.1	51.0	48.2	47.7	43,3
EGFRØ9.MØ9	19152:42,95	0,2	1574.4	81.5	53.1	44.9	46.1	48.3	45. ī	48.2	48.2	47.4	49.8	47.3	46.0	44.2	43,2	39.8
EGFRØ9,M10	19152143.71	0,2	1818.7	72.3	48,2	40.6	45.9	47.9	46.3	50.3	48.1	44.1	45.6	42.3	40.3	39.5	.35.6	34.0
EGFRØ9, M11	19152143.72	0.1	1821,8	62.0	49.1	42,2	39.2	36.8	42.3	44.2	46.9	49.1	47.3	48.5	46.6	42.6	39,9	36.1
EGFR09,M12	19152143.73	-0.1	1824.8	75.1	47.6	49.6	44.7	48.3	51.5	50.3	54.1	52.6	53.4	48.3	47.3	45.9	43,6	41.2
EGFR09.M13	19152139,80	1.3	248.1	98.5	80.1	75.8	78.3	75.4	80.6	86.0	89.2	90.3	90.0	88.7	88.9	88.8	87.0	85,0
EGFR09, M14	19152139,81	1.0	251.1	92.0	79.0	82.1	83,2	81.1	78.6	80.8	77.0	79.4	74.7	75.3	70.2	70.7	68.8	66.9
EGFR09, M15	19152139.83	-0.8	254.1	93.3	81.7	84.9	83.7	82.9	81.9	83.7	83.4	80.9	79.7	80.2	76.4	74.0	72.9	71.9
EGFRØ9.M16	19152139,06	52.6	5.5	111.4	103.4	103.1	103.3	103.8	101.4	99.7	94.5	97.6	98.0	96.3	95.8	95.1	95.7	96.6
EGFRØ9, M17	19152139,06	51.7	5.6	112.0	105.0	103.9	103.5	104.8	102.1	97.8	94.8	98.8	97.0	95.7	96.6	96.1	96.2	96.9
EGFRØ9.M18	19152142,60	0.4	1386.1	69.5	56.5	54.1	50.4	53.5	55.0	54.3	52,9	55.7	54.6	54.5	51.1	49.2	47.6	43.2
EGFRØ9, M19	19152144.10	0.2	1623.7	64,9	52.1	45.7	45.2	48.4	50.4	49,5	50.8	51.0	50.0	48.5	45.8	43.9	41.1	38.8
EGFRØ9.MZØ	19:52:44.88	0.1	1871.1	64.5	50.1	46.5	48.2	52,4	53.6	56.1	52.9	53,0	48.3	49.6	46.5	46.8	40.8	39.9

APPENDIX C

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1,6	2.0
	TIME	(deg)	(m)															
FGFR (A. HA)	19156124.78	4.9	217.3	100.8	70 6	7 CA	87 A			_	0E 0							*****
, , -	19156124.79	4.5	220.2															
•-•		•						87.6										
	19:56:24.79	2.4	555.6					91.1										
EGFR10.M04	19156125.45	2.3	437.4	83,2	74.5	72.9	74.5	71.0	71.0	68.6	66.4	68.4	71.0	69.1	66.7	65.Ø	63.7	62.0
EGFR10. MØ5	19:56:26.35	1.4	731.5	74.7	62.6	61.7	57.4	55.0	52.0	50.7	54.1	56.1	55.4	57.2	56,9	55.7	52.4	50.0
EGFR10. M06	19156126.50	1.1	886,9	72.3	62.4	65.9	52.4	49.8	51.7	51.0	49.4	55.7	56.1	58,0	52,3	53.6	52.9	48.3
EGFR10.MØ7	19:56:27.19	0.9	1111,9	72.5	62.3	64.0	55.8	50.3	52.5	50.5	50,8	52,0	55.0	53.3	53.6	52.8	50.3	46,7
EGFR10.MØ8	19:56:27.93	0.7	1352.7	67,3	54.7	54.6	53.4	46.5	47.9	47.8	52.0	52.6	53.9	54.2	54.1	52.3	50.2	46.5
EGFR10, M09	19:56:28.60	0.6	1571.9	64.7	54.7	49.9	51.1	49.5	48.0	46.9	48.7	49.5	47.8	50,7	47.8	45.5	43.4	39,9
EGFR10,M10	19156129.35	7.6	1815.6	64.3	42.3	42.8	46.2	48.7	47.A	48.7	47.1	44.5	43.6	40.6	39.1	36.3	35.5	33.0
EGFR10.M11	19156129.36	0.5	1818.6	59.8	48.6	40.6	43.9	41.7	45 • t	43.6	47.0	46.9	46,9	49.1	48.2	45.9	41.6	37.5
EGFR10.M12	19156129.37	0.3	1821.6	72.0	51.2	49.0	52.0	50.3	57.3	52.8	59.2	60.6	55.5	53.3	56.5	52.6	48.5	44.6
EGFR10.M13	19:56:25.55	4.3	250.6	99.9	79.3	81.0	80,3	80,6	89.1	92.5	94.2	85,8	91.1	87.2	88.9	87.6	86,7	81.5
EGFR10.M14	19156125,56	3.9	253.5	102.0	81.5	86,8	91.9	94.7	91.2	90.2	93,5	93,0	91.4	88.7	86.2	84.6	82.0	73,9
EGFR10.M15	19156125.56	2,1	256.0	99.1	81.2	82.7	84.4	86.2	87.7	90.6	92.0	93.0	89.8	87.5	85.9	86.3	84.6	81.5
EGFR10, M16	19156124,94	55.8	21.0	113,0	99.7	101.5	101.2	102.9	93.0	90.5	97.6	107.5	105.7	101.9	95.5	96.2	97.9	97.3
EGFR10.M17	19:56:24.94	55.6	21.1	113,3	100.4	100.9	102.2	102.6	91.4	92.8	99.4	109.6	105.5	99.7	96.4	95.9	98.8	97.8
EGFR10, M18	19:56:29,09	0,7	1402.4	72.4	59,6	56.4	54.4	53.8	58.7	58.2	56.7	53.2	51.8	54.5	50,2	48.8	45.9	43.0
EGFR10.M19	19156129.75	0.6	1621.6	70.8	50,5	51.2	45.4	47.9	52.4	58.8	54.5	51.3	48.9	48.0	45.3	43,3	40.2	37.9
EGFR10.M20	19:56:30,51	0.5	1968.3	62,2	54,6	48.1	49.1	47.4	50.4	51.6	49.2	49.0	48.9	47.3	45.0	43.3	41.5	38,9

FILENAME	RECEIVE	BETA	5 R	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0,63	0.79	1.0	1.3	1,6	2.0
	TIME	(deg)	(m)															
EGFR11.M01	20: 0: 2.70	5.8	211.0	99.3	79.4	80.7	85,6	89.7										70.6
EGFR11. MØ2	20: 0: 2.71	5.4	213.9	96.9	84.6	83.4	84.8	85.8	85.1	86.0	88,2	86.8	86.9	85.3	84.6	84.7	83,5	81,9
EGFR11.403	20: 0: 2.72	3,2	216.1	98.8	71.7	79.8	81.8	85.9	91.6	88.1	91.1	91.0	88.3	87.4	86.2	85.1	85.0	82.5
EGFR11.M04	20: 0: 3.41	2.6	432.1	83.5	74.9	73.4	71.2	69.1	65.6	64.9	69.6	70.4	70.3	69.1	70.0	70.4	69.6	65.1
EGFR11, MØ5	20: 0: 4.35	1.6	728.0	75.1	62.4	64.1	54.9	54.6	51.4	50.5	55,2	54,3	58.0	54.6	54.0	53.2	51.7	52,0
EGFR11. MØ6	20: 0: 4.52	1.3	884.6	71,2	53,9	61.1	60.3	57.9	51.2	50.8	55.8	54.1	55.8	57.2	54.0	52.8	50.1	47.8
EGFR11. MØ7	20: 0: 5,25	1.0	1111.0	66,9	53.7	62.0	53,9	54,8	51.5	49.0	50.5	49.7	51.8	52.2	50.9	48.8	47.3	42.9
EGFR11. MØ8	20: 0: 6.02	0.8	1353.3	66.6	56.9	55.7	51.4	48.8	44.5	48.3	53.1	54.3	51.4	51.5	52.0	50.4	49.1	46.5
EGF911. MØ9	201 01 6,72	0.7	1573.8	69.5	49.1	53.1	43.7	46.6	46.0	46.9	46.6	50.4	50.6	49.2	46.5	45.3	42,3	39.6
EGFR11.M10	20: 0: 7.53	0.7	1818,9	73.3	49.4	43.3	44.7	46.6	43.A	49.4	46.7	46.4	46.2	40.4	38.3	36.4	35,6	32,9
EGFR11.M11	20: 0: 7.51	0.6	1822.0	65.6	47.0	50.2	45.4	41.3	39.9	43.5	44.3	45,9	48.4	49.8	48.6	44,8	42,6	37.4
EGFR11.M12	20: 0: 7.52	a . 4	1825.0	69.7	46.5	45.2	52.4	47.6	54.9	52.6	57.1	55.7	52.6	53.9	51,5	50.9	46,3	42.9
EGFR11.M13	20: 0: 3.48	5.0	243.7	81.0	57.6	57.9	57.3	58.1	57.3	59.3	58,9	56,8	56.6	56.2	56.2	56.8	56.4	54.9
EGFR11.M14	20: 0: 3,48	4.6	246.6	87.2	54.6	54.0	52.0	53,4	53.7	53.6	52.8	54.2	54.7	52.9	51.6	53.4	50.0	49.5
EGFR11.M15	20: 0: 3.49	2.8	248.9	67.8	61.1	57.5	56.3	56,8	57.4	57.3	58.4	58.7	58,4	57.1	56.3	57.3	56.3	54.8
EGFR11.M16	201 01 2.92	55.9	24.0	88.2	80.2	80.6	80,2	82.8	80.9	80.3	80.9	80.3	81.2	81.2	80.3	81.1	81.1	79,9
EGFR11.M17	201 01 2,92	56.0	24.0	90.1	80.4	80.3	81.7	84.8	80.9	82.7	81.3	81.0	81.8	80.7	80.1	80.8	80.7	79.8
EGFR11.M18	201 01 7.16	0.8	1402.2	70,6	54.7	59.2	55.1	56,5	60.3	55.4	54.8	54.7	53.7	52.1	49.8	47.8	44.2	42.2
EGFR11.M19	20: 0: 7.86	0.7	1622.7	69,0	47.5	52,8	48.9	52,4	53.1	54.5	56,3	54.1	53,2	49.6	48.8	46.4	43.3	39.5
EGFR11,M20	20: 0: 8.66	0.6	1870.9	64.5	53.2	53,3	48.5	53.4	50.2	52.5	54.1	52,7	51.2	49.2	47.9	44.6	42.4	39.5

FILEN	NAME	RECEIVE TIME	BETA	5 R	OSPL	0.10	0.13	Ø.16	0.20	0.25	0.32	0.40	0.50	0.63	Ø.79	1.0	1.3	1.6	5,8	į
			(deg)	(m)							~									
EGFR12	. MØ1	20: 3:59.73	5.9	215.7	97.7	79.1	83.0	81.5	84.9	89.6	91.1	91.6	90.0	85.4	77.4	74.4	71.7	69.0	63.5	i
EGFR12	2.MØ2	20: 3:59.73	5.5	218.5	97.5	78.5	77.0	79.2	80.7	87.5	87.0	87.6	90.5	86.6	84.7	85.3	85.7	83,9	81.3	
EGFR12	. Mø3	201 3159.74	3.4	220.7	95.2	80,9	83,6	80.5	82.7	83.A	87.3	88,2	87.8	82.6	77.4	80.4	79.6	75.4	77.8	
EGFR12	. Ma4	201 41 0.41	2.8	435.7														62,8		
EGFR12	. Ma5	20: 4: 1.31	1.7	730.1														54.1		
EGFR12	, M26	20: 4: 1.47	1.4	885.7														55.4		
		20: 4: 2.16	1.1	1110.9														50.1		
		20: 4: 2.91		1352.0														47.8	_	
		201 41 3,59		1571.5																
EGFR12																		45.8	-	
	-			1815.4	70.9													35,4		
EGFR12		- '	3.7	1818.4	66.2	48.7	43,4	46.5	46.8	51.2	45.0	47.5	49.2	49.1	50.4	50.8	45.9	42.0	36.6	
EGFR12	.M12	201 41 4.36	0.4	1821.4	76.8	52.2	48.9	59.2	59.0	56.a	60.9	60.7	62.0	55.0	56,8	53.9	50.9	47.2	43.0	
EGFR12	.M13	20: 4: 0.49	5.2	248.8	97.8	76,2	76.6	85.7	88.3	87.	90.9	86.5	88.3	88.4	84.7	87.4	85.9	86.7	83,7	
EGFR12	.M14	20: 4: 0.50	4.8	251.7	101.4	82.8	84.3	88.7	89.2	89.0	91.8	92.0	93.3	90.1	89.8	85.6	81.4	77.9	78.5	
EGFR12	.M15	20: 4: 0.50	3.0	254.0	105.3	80.7	82.5	89.5	86.4	93.4	96.1	95.7	95.0	96.2	93.9	93,8	95.3	94.6	90.2	
EGFR12	. M16	20: 3:59.91	57.4	25.1	124.6	89.9	100.1	106.9	111.0	115.4	110.8	114,6	114.4	116.3	114.5	113.1	111.6	110.6	109.2	
EGFR12	, M17	20: 3:59.91	57.3	25.2	124.7															
EGFR12	.M18	20: 4: 4.04	0.9	1401.5														43.0		
		20: 4: 4.72	-	1621.0														44.4		
		20: 4: 5.48		1868.0														44,4		

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0,25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2,0
	TIME	(deg)	(m)															
FGFR13 Mg1	21: 2:30.64	5.5	204.9	07 A	0 / 7	81 /I	81 7	07 Z		-			8/1 3				72.	*** **
	•		_										84.2					
	21: 2:30.65	5.1	207.8	101.1	82,3	84.1	83.0	85,5	88.3	88.0	88.8	90.9	89.4	90.4	91.1	89.3	90.0	89.5
EGFR13.MØ3	211 2130.66	2.9	210.1	103.3	75.9	78.1	87.6	90.5	92.A	94.5	91.3	95.7	93,2	92.7	90.8	90.9	89.5	87,0
EGFR13.MØ4	21: 2:31.38	2.5	428.0	87.6	75,4	7,7 . 2	72.6	68.5	66.8	63.1	69.7	72.9	74.0	72.4	73.0	71.8	75.4	76.1
EGFR13, M05	21: 2:32.37	1.5	726.3	75.6	62,3	65.1	57.7	58.4	62.3	50.7	63.0	65.4	68.9	68.1	66.2	61.5	64.7	63.4
EGFR13.M06	211 2132,60	1.2	884.7	81.1	66.7	59.4	57.8	62.5	64.3	51.2	64.9	69.6	72.3	72.9	73.6	71.7	65,9	62.7
EGFR13,M07	211 2133,36	8.9	1112.9	73,6	58.8	63.9	55,9	52.6	56.4	54.9	55.9	60.1	65.3	64.1	64.0	58.0	56.7	55,4
EGFR13.MØ8	211 2134.17	0.8	1357.3	72.2	55.6	52.8	54.2	52.6	55.A	56.5	58.6	61,6	61.7	62.2	62.9	62.7	60.8	55.3
EGFR13.M09	21: 2:34.91	0.7	1579.6	70.1	49.1	47.2	50,3	48.4	53.9	56.1	56.9	61.5	63.2	60.3	57.8	59.3	57.7	52,3
EGFR13,M10	211 2135,73	0.6	1826.8	68.0	51.5	46.6	46.6	49.7	49.4	45.6	45.7	48.5	49.2	43.6	43.2	41.8	39.9	38,8
EGFR13.M11	211 2135.73	0.6	1829.9	67.0	48,0	45.4	48.2	43.7	48.6	50.8	52.4	57.1	56.8	55.0	158.4	58.3	52.6	47.3
EGFR13, M12	211 2135,74	0.3	1832.9	73.5	45.3	47.6	48.0	53.4	54.6	55.9	56,0	53,7	57.3	55.8	53.1	49.1	46.1	41.6
EGFR13,M13	21: 2:31.35	4.8	236.9	97.9	76.7	78.6	83.5	85.6	89.5	91.5	85,8	87.0	88.5	87.3	89.4	88.0	86.0	79,4
EGFR13.M14	211 2131.36	4.4	239.8	99.8	82.3	83.8	88.4	90.8	92.9	90.7	90.0	90.3	89,3	88,8	85.4	84,6	79.8	75,1
EGFR13.M15	211 2131,37	2.5	242.3	100,9	80.7	84.6	89.7	92.4	93.6	92.3	91.2	89.1	89.9	90.1	88.9	85.9	84.1	80,8
EGFR13,M16	21: 2:30.84	46.3	25.6	107.1	94,6	98,2	95.1	97.9	91.7	89.7	89.0	94.1	100.0	100.6	92,9	88.1	91.0	89.1
EGFR13.M17	211 2:30.84	46.6	25.5	105.0	97.8	96.9	96.5	96.9	94.4	91.1	84.9	88.1	94.2	95.7	92,3	5,88	86.3	88,6
EGFR13, M18	211 2135,23	0.8	1405.1	81.1	55.4	59.6	67.1	67.8	65.4	69.7	70.7	69.7	66.4	62,8	60.6	55.1	54.9	48,3
EGFR13,M19	211 2135,96	0.7	1627.4	76.2	53,4	50.6	57.9	63.4	64.9	65.4	64,6	63.3	57.8	55.7	56.2	51.5	49.6	43.3
EGFR13.M20	21: 2:36.80	0.6	1877.7	77.8	53.4	53.0	58.3	67.2	68.1	70.2	69.2	69.6	68.8	70.3	66.6	59.8	54.8	48.6

APPENDIX C

FILENAME	RECEIVE Time	BETA (deg)	SR (m)	93PL	0.10	0.13	0.16	0.20	•	-	-					1.3	1.6	2,0

EGFR14.MØ1	21: 6:19.69	5,5	217.1	102.6	87.3	87.4	86.7	93.6	94.7	95.6	96,9	93,2	89.2	83.8	80.3	77.7	73.5	71.1
EGFR14.MØ2	21: 6:19.78	5.1	220.0	102.7	87.0	86.9	86,2	90,5	92.7	93.5	94.4	92.4	92.9	92.1	90.6	89.6	89.2	88,7
EGFR14.MØ3	21: 6:19.70	3,0	222.3	104.1	86,6	91.3	89.5	86,5	87.8	93.0	97.0	97.7	91.6	93.7	90.0	93.9	91.2	87.4
EGFR14.MØ4	211 6120.36	5.6	437.1	89.0	83.0	84.5	77.4	76.3	72.5	68.4	71.8	74.9	71.9	71.5	70.8	74.3	72.5	74.5
EGFR14, MØ5	211 6121.27	1.5	731.3	78.8	66.8	66.7	64.9	60.4	63.5	56.9	63.2	63.6	63.7	63.2	64.9	66.5	65.1	62,3
EGFR14. MØ6	21: 6:21.41	1.3	886.7	77.6	66.8	64.6	61.5	55.8	57.3	57.2	66.3	61.0	65.2	64.8	64.6	64.3	63.4	61.3
EGFR14.M07	21: 6:22.10	1.0	1111.7	76.9	65.3	59.4	61.6	55.1	56.7	59.6	55.3	60.3	65.3	63,1	64.2	63.7	60.0	55.4
EGFR14.MØ8	21: 6:22,84	0.8	1352.7	80.4	66.4	64.8	52.8	54.9	59.6	61.6	66,2	68,3	65.0	71.3	65.8	70.4	65,5	62,4
EGFR14, MØ9	21: 6123,52	0.7	1572.0	75.0	58,6	58.0	55.5	49.2	51.2	56.7	59.8	61.7	62.1	59,9	59.0	59.4	58.0	56.6
EGFR14.M10	211 6124,27	0.7	1815.7	64.6	52.3	50.4	51.1	54.0	50.9	52.5	53.4	52.0	50.1	46.1	42.5	44.7	41.6	38.6
EGFR14.M11	21: 6:24.27	0.6	1818.7	67.1	50,7	48.3	50,2	49.7	52.2	53.1	51.7	58,5	59.1	58.0	56.4	54.8	52.8	49.8
EGFR14.M12	21: 6:24,28	0.4	1821.7	75,7	48.6	47.6	57.4	57.1	60.1	55.5	60.4	65,6	65.1	62,9	61.7	57.8	53.8	48.4
EGFR14.M13	21: 6:20.47	4.7	250.3	104.9	81.0	72.4	85.3	92.1	96.2	98.6	90.1	95,2	92.6	97.7	94,8	92.2	91.9	87.4
EGFR14.M14	211 6120,48	4.4	253.3	105.9	87.0	90.9	93,2	91.9	95.4	96.2	97.5	99.2	95.7	93,3	86.6	89.8	91.6	90.5
EGFR14.M15	21: 6:20.48	2.6	255.6	109.7	88,5	91.1	94.0	93,6	95.4	96.9	99.3	101.4	100.2	101.4	99.3	97.9	96,9	95,3
EGFR14.M16	211 6119.88	56.4	23.4	117.5	101.7	104.5	98,5	91.8	102.5	109.7	111.2	109.3	102.4	107.4	104.5	106.9	102.6	100.4
EGFR14,M17	211 6119,88	56.3	23.5	103.6	95.0	98.0	94,8	94.5	94.7	89.4	89.4	88,6	88.0	90.2	93,0	92.6	90.3	86.3
EGFR14.M18	21: 6:24.01	2.8	1402.3	78.1	62.3	61.6	65,5	63,3	65.5	70.8	69.4	64.5	65.0	60.7	59.0	59.4	57.7	55.4
EGFR14.M19	21: 6:24.68	0.7	1621.6	71.8	62.0	58.0	58.8	57.7	60,3	61.4	62.8	59.9	59,6	56.1	56.2	53.6	50.7	48.6
EGFR14.M20	21: 6:25,45	0.6	1868.4	71.9	60.1	61.0	57.8	59.5	57. a	62.7	60.9	57.8	57.9	55.9	54.3	52.1	51.3	45,8

FILENAME	RECEIVE	BETA	\$R	OSPL	0.10	0.13	0.16	0,20	0.25	0.32	0.40	a,5a	0.63	Ø.79	1.0	1.3	1.6	2,0
	TIME	(deg)	(m)															
EGFR15, M21	211 9153,99	5,2	205.3	100.6	81.1	82,2	88.2	91.3	91.7	93.8	93,8	92.0	P7.4	80.9	77.4	76.7	73.4	71.7
EGFR15.MØ2	21: 9:54.00	4.8	208.3	102.2	83,5	83.9	85.7	88.2	90.9	89.0	94.0	92.7	90.2	90.1	92.0	90.6	90.0	88.5
EGFR15.MØ3	211 9154.21	2.6	210,6	104.7	73,8	85.3	92.8	95.4	96.2	92.1	91.5	97.0	95.4	93.1	90.6	93.6	94.3	88.9
EGFR15. MØ4	211 9154,71	2.3	427.2	88.5	75,2	76.7	77.0	67.5	66.1	64.9	69.9	74.9	76.1	74.9	79.2	81.7	79.5	72.1
EGFR15, MØ5	211 9155.66	1.4	723.7	78,9	67.3	65.6	67.1	60.6	56.A	55.1	61.9	66.1	71.4	68.3	65.8	. 67.5	66.4	64.0
EGFR15, MØ6	211 9155.85	1.1	880.9	77.1	68,3	63.8	63.8	65.2	58.3	59.0	60.6	60.8	66.6	68.0	65.2	64.7	66.3	62,6
EGFR15.M07	21: 9:56.59	a.9	1107.7	76.7	62,9	64.0	60.0	58.9	58.3	60.1	58.3	56,2	57.9	58.9	59,9	58,6	59.0	57,0
EGFR15.MØ8	21: 9:57.37	2.7	1350.6	78.6	65,9	57.9	53,9	52,6	57.5	56.9	61.5	61.5	62.6	66.4	66.3	66,2	63.7	59.4
EGFR15.Ma9	21: 9:58.09	8.6	1571.6	73.3	54.5	52.4	51.0	49.6	46.A	50.5	55.0	55.6	56.2	56.9	55.6	55.6	53.0	49,4
EGFR15.M10	211 9158,88	0.6	1817.3	66.5	53,0	51.8	48.7	52.4	51.7	55.4	55.7	54.3	52.1	53.1	49.8	47.5	46.4	43,6
EGFR15.M11	21: 9:58.89	0.5	1820.3	68.8	48.8	44.1	44.9	45.5	48.5	54.1	59.2	58.7	59.9	62.1	58.9	57.7	57.6	53,1
EGFR15.M12	21: 9:58,90	0.3	1823.3	71.1	43,3	48.0	54.9	54.2	58.3	54.6	54.7	59.7	59,2	55.6	55.8	52.3	50.2	46.3
EGFR15.M13	21: 9:54,77	4.5	238.1	103.8	83,6	80.8	78.9	81.1	88.6	97.5	97.9	93.1	90.0	94.3	90.4	93.0	93.2	88.7
EGFR15, M14	21: 9:54,77	4,2	241.1	106.6	87.1	87.5	88.0	95.7	97.A	98.9	97.5	97.3	97.2	96.4	95.1	93,5	93.3	89.7
EGFR15,M15	21: 9:54.78	2.3	243.6	108.1	86,2	88.0	88.8	96,2	98.4	99.7	98.4	97.5	98.0	96.5	97.3	96.6	97.0	95,2
EGFR15.M16	21: 9:54.23	48,5	23.5	112.9	98.1	99.8	98.8	97.7	94.9	92,3	102.9	104.4	107.5	101.9	98.6	100.2	96,2	95,7
EGFR15, M17	21: 9:54,23	48.8	23.4	106.4	94,9	103.1	93.4	91.8	91.R	88.4	88.9	88.0	87,5	87.3	85.8	86,7	87.0	85,5
EGFR15. M18	21: 9:58,56	0.7	1402.1	78.8	58,2	56.8	61.0	64.8	67.B	66.8	68.2	66.0	62,3	61.9	56.8	57.8	54.9	49.1
EGFR15. M19	21: 9:59,29	0.6	1623.6	65.8	54.5	56.5	53,5	52,3	54.6	54.9	55,8	53.7	53,5	51.6	50,5	48.8	47.0	43,3
EGF915. M20	21:10: 0.10	0.5	1872.9	71.2	50,9	52.3	57.3	62.3	62.1	62.2	62.3	63.0	61.8	60,0	61.4	58.4	52.5	50.0

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	9,16	0.20	0.25	0.35	0.40	0.50	0,63	и.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
FGFR17.MA1	21:17:36,15	10.6	214.1	99.4	86.2	88.2			-		90.1						79.1	80,3
•	21:17:36.16		216.8								81.5							
	21:17:36,15	7.9	218.1	100.5	-													
- •	21:17:36.82	5.0	433.0								75.4							
	21:17:37,74	3.0	727.6								62.3							
-	21:17:37.91	-	883.6	_	-						63.0							
-	21:17:38.62	-	1109.3								60.1							
	21117139,38	•	1351.0								60.8							
			1571.1								57.4							
	21:17:40.07										52.8							
	21117140.84		1815.7								51.4							
- •	21:17:40.85		1818.7															
	21:17:40.86		1821.6								60.2							
• • • • • • • • • • • • • • • • • • • •	21:17:36.90	9.1		101.2														
EGFR17.M14	21:17:36.91	8.7		99.9														
EGFR17.M15	21:17:36,90	6,9		104,4														
EGFR17.M16	21:17:36.50	56.9		118.3														
EGFR17,M17	21117136,50	56.9	45.1	100.5	91.1	96.6	92.1	92.6	92.6	85,5	82,2	83.4	87.7	88.4	83,3	83,0	86.1	82.5
EGFR17, M18	21:17:40,50	1.5	1400.2	79.0	62.3	64.8	62.6	71.0	72.6	71.1	69.1	63,9	62.4	58.1	57.0	59,4	56,9	53,5
EGFR17.M19	21:17:41.19	1,3	1620.2	75,8	60.0	63.0	62.4	64.6	61.4	65.6	67.6	68,4	67.9	61.9	58.5	58.3	55.5	51,0
EGFR17, M20	21:17:41.98	1.2	1867.9	70,5	49.1	50.1	54.9	56.7	62.1	62.7	63,8	63.9	56.6	53.4	49.5	50,2	45.6	43.0

FILENAME	RECEIVE	BETA	5 R	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	2.40	0.50	0.63	0.79	1.0	1.3	1.6	2,0
**********	TIME	(deg)	(m)															
EGFR18.MØ1	21120158,28	10.1	216.1	99.4	84.5	86.9							84.2					
EGFR18.MØ2	21:20:58,29	9,6	218,9										91.1					
EGFR18, MØ3	21:20:58.29	7.5	220,2	103,9	80.8	85.1	89.4	90.5	86.7	96.8	94.1	97.8	94.9	93,5	91,2	92.7	88.7	87.1
EGFR18.MØ4	21:20:58.96	4.8	435.3										84.3					
EGFR18.MØ5	21120159,89	2.9	730.0										75.6					
EGFR18, MØ6	21:21: 0.06	2,4	886.2	85,2	62.2	65.8	66,2	61.5	65, 3	65.0	72.6	72.0	76.2	77.4	74.0	72.8	70.0	67.8
EGFR18.MØ7	21:21: 0.77	1.9	1112.0	76.7	62.1	64.4	62.5	63.0	64.a	62.6	61.9	63.4	65.1	65.3	65.6	66.7	60,5	57.8
EGFR18.MØ8	211211 1.53	1.6	1353,8	83.1	65,0	71.3	64.5	60.8	56.1	56.2	58.8	64.3	66.4	65.8	68.6	66.5	65.3	59.6
EGFR18, MØ9	211211 2.23	1.3	1573.9	75,3	54.6	58.2	56.6	52.6	54.ã	54.9	57.2	60,3	61.2	60.0	61.2	57.3	54.5	50,8
EGFR18.M10	211211 2.99	1.2	1818.6	68,3	52,6	53.8	53,5	50.9	51.6	50.0	53.3	50.1	45.9	46.3	45.9	45.9	41.8	39.8
EGFR18,M11	21:21: 3.00	1.2	1821.6	66.9	50.5	50.7	49.6	44.8	43.4	46.4	49.6	54.6	53.8	53.0	51.7	52.6	49.9	45.2
EGFR18,M12	21:21: 3.01	0.9	1824,5	71.7	44.1	50.5	56,0	50.6	57.9	60.9	64.7	63.5	62.2	56.9	55.4	55.8	46.7	45.3
EGFR18,M13	21:20:59.02	8.7	248.5	101.0	78,6	82.6	89.1	91.6	85.6	94.6	90.9	91.3	90.4	91.8	88.3	87.5	85.1	82.4
EGFR18.M14	21120:59.04	8.3	251.3	100.4	85.4	89.0	87.4	92.2	92.0	91.8	91.7	90.0	82,6	76.9	84.7	89.0	87.4	84.1
EGFR18,M15	21120159.03	6.4	252.8	100.4	80.6	79.8	84.8	89.1	88.3	91.3	90.7	90.9	91.1	91.4	89.9	89.7	87.6	89.1
EGFR18,M16	21:20:58.60	57.0	43.0	112.1	94.4	97.5	93.6	86,9	97.3	105.0	106.7	103.7	102.5	104.2	99.6	99.0	97.3	96.7
EGFR18, M17	21:20:58.60	57.1	43.0	107.6	88.9	98.3	93.0	88.4	83.8	90.9	100.6	102.6	100.0	91.6	92,0	90.6	95.2	91.7
EGFR18.M18	21:21: 2.65	1.5	1402.8	75.7	58.8	65.6	63.9	63.0	61.2	59.3	61.2	64.2	62.2	63.6	63,2	57.5	54.4	52.5
EGFR18.M19	211211 3,34	1.3	1623.0	70.6	56.3	60.7	54.1	57.0	61.7	63.4	64.3	60.1	57.4	57.5	53.6	52.8	49.0	46.1
EGFR18.M20	21:21: 4.12	1.1	1870.7	73.2	64.4	61.2	58.8	66.3	63.4	64.0	58.8	58.5	61.2	59.4	54.2	50.3	50.8	46.6

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	P.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFR19. MØ1	21125:58.45	18.7	219.8	100.6	88.2	85.5	89.5				-	90.6	91.7	91.3	89.3	88.9	88.3	86.4
	21:25:58.45	-	222.1	101.1			-				· -	-		-		-	•	•
	21:25:58.43		221.8	-			_	-		_	•	-		95.1			•	-
	21125159.09	9.2	433.4											83.6		-	-	-
	21:26: 0.00	5.5	726.5	-	-	-	-	-	- •			_	•	72.9	•		•	
	21:26: 0.19	4.5	882.5											69.6				
• •	21:26: 0.90	-	1128.2											71.1				
	211261 1.67	-	1350,2	-	=		-				=		-	69.1	-	-	•	•
_	211261 2.37		1570.5											62,7				
	211261 3.15	-	1815.6											48.9				-
• • •	211261 3,16	-	1818.6	•	-	-	-	•			•	-		56.7		_	•	
	211261 3.16		1821.3	•		-								53.7			_	-
	21:25:59.16			102.1														
	21:25:59.17			100.0	-		-	-			_	•	•	-	-	-	-	-
	21:25:59.16	•	253.1		-							-	-	87.6	•		-	-
• •	21:25:59.05		82.9	-	-			-		-	-	-	-	103.6	•	•	-	•
	21:25:59.05	-	82.9	•	•	-	•	-	•		•		•	•	-	•	. •	•
	211261 2,77		1398.9											63.5				
	21:26: 3.47		1619.3											61.3				
	21:26: 4.26		1867.4			-	-			-	•		•	58.8	-	-	•	•
20111278 20				, 200	2011	22.0	2011	3.44	UEIM	0 2 6 4	27,44	0.07	7 7	30.0	2294	40.7	-/ 1 4	45,0

FILENAME	RECEIVE	BETA	9 २	OSPL	0.10	0.13	3.16	0,20	R. 25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
***********	TIME	(deg)	(m)														•	
ECEDDA NO.	24.20.00																	
	21:29:40.24	21.9	228.6	100.6	85,6	86.9	90.1	88.4	90.2	87.0	88.5	90.6	92,1	90.0	86.2	86.1	85.2	86.5
EGFR20.M02	21:29:40.24	21.4	230.8	99.3	84,5	85.4	83,3	78.6	81.9	86.4	92.6	94.0	93.8	84.3	85.6	85.6	81.8	84,1
EGFR20.M03	21129140.22	19.4	229.7	102.4	83.0	79.0	89.4	88.4	92.6	90.9	93.1	96.0	93,2	91.9	90.6	91.1	87.3	85.7
EGFR20.MØ4	21:29:40.84	11.1	438.3	89.3	75,9	78.9	75.3	72,8	72.5	75.6	79.1	83.3	82.8	80.8	76.0	73.3	70,9	69.5
EGFR20.M05	21:29:41.73	6.6	729.5	82.1	67.6	66.1	66.8	63.5	65,4	69.8	69.5	70.5	74.4	70.8	67.5	67.6	65.4	59.8
EGFR20.M06	21:29:41.91	5.4	884.7	81.7	62.7	65.5	64.1	66.3	64.0	66.4	66,4	67.2	69,3	69.0	71.1	69,5	66,0	59,1
EGFR20. M07	21:29:42.61	4.3	1109.7	82.2	69.9	68,8	71.7	68.3	69.7	69.5	70.2	67.8	71.1	71.8	69.8	72,0	68,7	64.6
EGFR20.M08	21:29:43.37	3,6	1350.9								76.2							
EGFR20, M09	21:29:44.05	3.1	1570.7	69.8	58,0	56,9	8,52	51.1	50.4	53.4	55.8	57.9	58.9	57.8	55.5	55.5	53.7	49.6
EGFR20.M10	21:29:44.83	2.7	1815.2	66.4							49.3							
EGFR20.M11	21:29:44.84	2.7	1818.2								49.3							
EGF920.M12	21129144.84	2.4	1820.9								65.3							
EGFR20.413	21:29:40.95	19.4	258.9	102.3	81,4						93.1							-
EGFR20.M14	21:29:40.96	18.9	261.2	102.7														
EGFR20.M15	21:29:40.94	17.1	260.7								86.8							
EGFR20.M16	21:29:40.94	57.7	100.5	107.1														
EGFR20, M17	21:29:40.94	57.7	100.4	107.0														
EGFR20.M18	21:29:44.47	3.5	1399.9			,					77.5						59.7	
EGFR20, M19	21129145.16	3.0	1619.8								68.5						-	
EGFR20, M20	21:29:45.93	2.6	1867.3								65.9							-
										-	-	- -	•		• .		- • • •	

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	ø.13	0.16	0.20	0.25	Ø.32	0.40	a.50	0.63	0.79	1.0	1.3	1.6	5.0
	TIME	(deg)	(m)						·									
EGFR21.MØ1	21:33:13,89	20.4	219.5	100.8													85.8	83.8
-	21:33:13.89		221.8						83.4									
EGFR21.MØ3	21:33:13.87	17.8	221.0	103.4	83.0	78.9	90.8	88,6	92.5	92.8	94.1	93.9	94.6	95.9	92.7	91.7	88.5	86,6
EGFR21.Ma4	21:33:14.55	12.0	432.8	96.5	75.8	77.1	80.9	76.3	76.1	81.4	87.7	91.0	89.9	87.9	83.7	82.2	81.4	78.4
EGFR21.MØ5	21:33:15.51	6.0	727.2	83.4	63.8	66,5	67.4	66.3	65.9	63.0	67.1	70.3	69.2	66.0	66.0	67.0	72.4	66.0
EGFR21.MØ6	21:33:15.71	4.9	884.5	85.9	66.9	65.1	69.1	66.3	68.Š	69.4	71.6	76,0	79.1	78.8	79.0	76.1	72.7	67.1
EGFR21.MØ7	21:33:16.46	3,9	1111.6	79.0	66.2	68.8	69.6	66.8	67.5	59.3	62.6	65.6	66.8	69.9	69.4	67.5	66,0	60.0
EGFR21.MØ8	21133117.27	3.2	1355.0	87.7	64.8	65.3	67.9	64.1	69.4	70.7	73.2	77.8	79.6	81.1	80.1	78.7	74.3	65.8
EGFR21. M09	21:33:17.99	2.7	1576.8	71.8	58,5	56.8	56,6	52.1	55.7	57.9	60.3	61.9	62,8	61.9	61.8	57.3	55.1	49.0
EGFR21.M10	21:33:18.81	2.4	1823.4	65,3	52.4	52,5	51.9	55,3	51.A	51.8	50.7	51.5	49,8	46.8	45.9	43.8	41.9	38,7
EGFR21.M11	21:33:18.82	2.4	1826.4	64.8	51.9	49.4	51.2	48.5	48.5	48.8	50.9	54.1	56,4	57.5	54.6	51.7	50,6	44.5
EGFR21.M12	21:33:18.83	2.1	1829.1	73.8	52.2	52.3	60,6	61.8	63.3	59.6	61.3	63.6	60.8	61.3	58.1	57.3	52.7	47.2
EGFR21.M13	21:33:14.62	17.9	249.3	102.2	78.2	79,6	89.6	85.5	92.9	92.3	92.5	95.1	95.6	93.7	89.8	89.0	88,6	86,0
EGFR21.M14	21133114,62	17.5	251.7	100.0	84.4	83.4	84.8	80.9	77.9	87.4	92.4	94.8	92.1	86.1	92,8	84.3	86,4	82.2
EGFR21,M15	21:33:14.60	15,6	251.5	94.9	75.5	78.4	79.6	84.5	83,0	86.6	85.2	85.9	86,0	85,7	83,4	79.8	78.4	74.6
EGFR21,M16	21133114.55	56.2	91.1	111.0	87.1	82.8	85,1	94.3	101.6	104.1	98.3	101.8	194,6	99.9	97.5	98.7	98.4	94.7
EGFR21.M17	21:33:14,55	56.2	91.0	98,8	90.0	87.0	86.8	84.2	76 • ī	81.4	90.1	94.0	91.9	83.3	83.3	81.1	86,3	82.0
EGFR21,M18	21:33:18,38	3.1	1402.9	80.5	68.1	69.3	72.1	70.3	67.i	68.1	68.6	70.6	70,4	63.6	60.8	60.6	58.1	52.5
EGFR21.M19	21:33:19.10	2.7	1624.7	81.4	64.0	68.9	72.2	71.9	74.3	75.9	75.6	66.5	64.1	63.4	58.0	58.6	58.0	51.6
EGFR21,M20	21133119.93	2.3	1874.3	77.4	62,3	65,0	67.6	71.9	70.6	69.6	66.3	62.7	59,4	60.0	56.9	55.0	50.3	46.t

														,					
FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2,0	
	TIME	(deg)	(m)																
EGFR22.Mai	21:36:49,55	34.7	264.3	00 7	70 (07 0				•									-
								87.3											
	21:36:49.55		265.7					85.1											
EGFR22,M03	21136149.52	32.6	265.0	101.0	78.6	89.9	89.1	91.1	90.9	91.7	92.0	92.5	93.1	89.0	86.5	86.4	83.4	80.2	
EGFR22.M04	21:36:50,02	19.1	454.7	93.8	73.1	75,6	72,0	76.0	78,5	85.5	87,7	85.6	78.4	84.6	82,0	79.7	78.3	76.4	
EGFR22.MØ5	21:36:50,88	11.6	738,5	83.1	67.6	69.3	67.4	64.3	67.3	74.2	77.0	75.4	71.6	69.0	67.9	68.5	66.9	62.0	
EGFR22,M06	21:36:51.08	9,6	892.7	86.3	68.7	70.8	71.9	67.5	69. p	74.5	78,2	79.9	77.5	73,2	69.8	70.7	63.9	65.3	
EGFR22,M07	21:36:51,79	7.7	1117.0	82.3	62.P	70.3	68.4	65.3	59.4	66.1	69.4	72.8	76.4	75.1	65.3	62,8	66,4	58,3	
EGFR22.MJ8	21136152.58	6.3	1358.4					64.3											
EGFR22.MØ9	21:36:53,29	5.4	1578.7					57.3											
EGFR22.M10	21136154.05	5.0	1838.9					61.9											
EGFR22.M11	21:36:54.06	5.0	1841.9	68.9	57.4	56,2	57.0	55.6	54.0	51.2	54.9	57,4	60.3	62.7	57,6	56.0	49.1	42.7	
EGFR22, M12	21:36:54.07	4.7	1844,1					67.2											
EGFR22. M13	21136:50.22	31.4	289.7	100.4	78.9	79.8	86.0	86.8	91.1	90.1	90.4	94.0	90.0	89.3	88.7	88.4	86.2	84.8	
EGFR22.M14	21:36:50.23	31.0	291.3	99.5	69.9	69.5	82.9	90.2	93.9	91.5	86.3	92.5	87.3	89.1	86.4	85.5	83.4	81,5	
EGFR22.M15	21:36:50.18	29,5	288.2	92.4	71.7	77.6	81.5	81,5	80.4	83.6	83.4	82.6	83.0	81.8	79.2	78.0	76.6	75.7	
EGFR22.M16	21:36:50.53	57.7	178.3	107.5	73.8	84.7	94.0	95,6	97.š	93.3	100.3	95.0	100.7	98.7	96.4	96.2	95.1	92,0	
EGFR22.M17	21:36:50,53	57.7	178.3	104.5	84.4	77.8	84.6	93,2	95.9	96.6	90.8	99.8	94.7	93.8	91.0	90.2	87.4	87.4	
EGFR22. M18	21:36:53,64	6.1	1406.2					69.3											
EGFR22.M19	21136154.36	5.3	1626.6																
EGFR22.M20	21:36:55.17		1875.1					69.3											

FILENAME	RECEIVE	BETA	SR	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	9.40	0.50	P.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFR23.Mu1	21:40:12.57	33.0	256.7	99.7	82.7	86.3	88.6	88.3		_	92.2						A2.2	A1.Q
-	21:40:12.56		258.2							-	91.5			_	-	•		
_ •	21:40:12.52		254.8	101.0				-		-	-	-			-	•		•
		-	_							-		•		-	-	•	- •	- •
EGFR23, M04	21:40:13.28		451.5								89.3						-	-
EGFR23.MØ5	21:40:13,99	10.8	738,5	83.0	70.0	66.7	66.1	65.8	69.3	71.2	75.1	78.5	74.4	71.1	71.4	72.4	65.P	61.6
EGFR23.MØ6	21:40:14.20	8,9	894.4	88.4	70.7	69.5	73.0	68,3	73.4	79.4	82.8	81.3	79.2	73.2	73.4	75,7	70.1	67.P
EGFR23. M07	21:40:14.95	7.1	1120.2	80,2	68.9	71.7	72.2	69.3	59,9	65.9	71.8	69.7	69.9	67.6	65.1	59.1	56.3	53,3
EGFR23.MØ8	21:40:15.77	5.8	1363.1	81.5	63.4	61.1	62.0	60.2	62.9	70.4	74.1	75.9	75.7	74.7	71.3	64.7	63.0	61.4
EGFR23, MU9	21:40:16.51	5.0	1584.8	73.6	62.8	63.5	63,9	59,9	62.5	65.6	64.0	62.6	65.5	64.9	60.6	57.4	55.4	47.8
EGFR23.M10	21:40:17.34	4.4	1831.6	69.9	57.2	62,3	60.9	61.2	59.A	59.1	58.5	56,3	56.8	57.3	52.8	50.4	45.2	41.5
EGFR23, M11	21:40:17.35	4.3	1834.6	68.5	57.9	58.7	57.0	55.8	55.3	53.2	55,9	57.9	60.4	61.2	56.7	51.0	46.4	42,5
EGFR23.M12	21:40:17.36	4.1	1836.9	75.2	57.3	66,1	67.9	67.1	64.3	66.9	65.5	61.8	59,9	61.2	57.0	53,3	50,6	44.4
EGFR23, M13	21140113.26	29.8	282.0	101.8	81.9	84.6	91.1	86.6	87.1	92.3	93.1	94.4	91.1	90.1	90.0	87.9	86,2	80.5
EGFR23. M14	21:40:13.26	29.3	283.7	99,3	74.1	67.9	81.9	88,5	95.5	90.5	84.0	90.4	89.0	89.0	85.3	83.6	80.2	80.0
EGFR23.M15	21:40:13.22	27.8	281.0	93,2	76,9	76.9	77.2	80.0	82.5	87.2	85,9	84.6	84.7	82.5	79.9	79.6	77.1	72.8
EGFR23.M16	21:40:13.53	57.0	166.0	108.8	72.3	84.2	92.2	95.5	99.4	93.2	103.3	99.3	101.7	99.8	96.5	95.1	94.4	89,9
EGFR23.M17	21:40:13,53	57.1	166.0	108.1	72.7	82.4	86.3	97.5	99.4	91.8	99.4	98.7	100.0	98.0	95.6	93.9	94.3	91.8
EGFR23.M18	21:40:16.86	5.7	1410.2	81.8	66.7	71.0	76.6	72.2	74.4	74.9	74.4	72.0	61.1	60.0	61.9	67.5	59,5	54.6
EGFR23, M19	21140117.62	4,9	1632,0	78.6	58.6	65,8	72.0	72.5	71.9	67.2	66.3	67.4	66.3	56.7	58.4	62,3	57.4	49.6
EGFR23, M20	21:40:18.46	4.2	1881.9	83,2	71.0	74.7	77.8	74.5	71.A	72.1	75.5	69.2	63.5	63.5	62,0	59.7	57.5	51.2

FILENAME	RECEIVE Time	BETA	SR (m)	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0,63	0.79	1.0	1.3	1.6	2.0
	1100	(deg)	(m)															
EGFR24.MØ1	21:43:27,49	32.9	270.2	102.6	81.4	81.4	89.8	89.8	92.3	93.9	95.5	91.9	91.9	91.3	90.1	90.7	88.9	89.1
EGFR24.M02	21:43:27.48	32.4	271.6	99.9	79,6	75.6	73.3	85.6	91.8	94.1	94.6	88.5	89.6	86.2	86.0	84.9	82.2	80.9
EGFR24.MØ3	21:43:27.44	30.8	268.3	100.3	79.6	86.8	84.3	88.4	88.7	94.8	93.1	91.7	90.4	88.6	85.6	86.7	83,9	81.5
EGFR24, MØ4	21:43:27,94	18.3	461.9	94.6	76,7	75.9	72.7	69.8	78.A	90.4	88.5	86.9	81.3	85.3	78.3	81.5	75,2	73.2
EGFR24.MØ5	21:43:28.75	11.3	744.2	87,3	66.2	67.5	71.8	66.7	69. R	74.0	78,2	82.7	82.3	77.4	73.3	73.7	69,1	63,9
EGFR24.M06	21:43:28.90	9.3	896.7	86.8	62.3	68.7	68.5	66.6	66.A	75.4	80,9	78.7	80.7	76.9	74.1	77.1	73.1	67.5
EGFR24. MØ7	21:43:29.58	7.4	1119.1	79.6	67.7	72.2	67.9	66.1	60.9	62.5	66,3	71.2	70.5	70.6	62,9	58.7	58,4	51.3
EGFR24.M28	21:43:30.31	6.1	1358.5	78.4	61.6	66,1	64.5	61.1	60.6	65.5	66,8	71.4	71.9	72.5	67.3	62.2	64.6	57.5
EGFR24, M09	21:43:30.98	5.3	1576.9	73,0	61.7	61.8	59.0	59.7	57.7	57.7	59,9	64.0	63,5	66.6	62.8	60.5	54.9	49.4
EGFR24.M10	21143131.74	4.6	1820.3	76.0	61.0	63.4	63.8	62.9	65. ü	68.1	67.4	66.4	66.7	65.8	64.7	60.2	53.9	45,8
EGFR24.M11	21143131,75	4.6	1823,2	78.4	56.5	60.7	58.6	55.3	57.ĵ	59.7	69.1	69.6	73.1	72.8	67.4	60.1	57.2	49.7
EGFR24. M12	21:43:31.76	4.3	1825.5	79.4	60,1	67.7	68.0	69.4	65.4	70.8	75.1	66.5	67.8	62.2	60.1	55.9	52.2	49.9
EGFR24.M13	21:43:28,16	29.7	296.9	99.0	85.4	84.5	86.1	89.3	88,9	88.6	91.5	90.3	88.7	87.1	87.4	86.7	84.9	81.0
EGFR24.M14	21:43:28.15	29,3	298.6	99.7	80,3	76.4	72.9	82.9	90.4	91.8	92,6	83.7	90.0	86.1	89.8	89.4	86.8	85.4
EGFR24.M15	21143128,11	27.8	295.8	103.3	85.5	85.9	91.2	92.0	93.6	97.5	95.9	94.2	91,7	94.4	93.0	91.5	90.2	88.4
EGFR24. M16	21:43:28.38	58.2	172.8	104.0	78.1	72.8	81.0	91.2	96.9	99.1	94,8	92.4	97.5	90.1	90.9	89.9	87.9	87.3
EGFR24,M17	21:43:28,38	58.2	172.8	98.4	82.6	83.5	75.5	74.2	74.7	87.1	93,1	93,6	85.3	90.3	83,3	82.4	77,9	79.4
EGFR24,M18	21:43:31.38	6. P	1407.5	84.8	68.3	70.1	74.1	79.0	77.3	76.1	74.6	75.1	73.2	65.6	61.5	59.1	61.6	54.3
EGFR24, M19	21:43:32.05	5.2	1626.1	78.7	63.3	64.1	66.3	66.5	70.6	70.9	72.7	68.7	66.6	59.1	56.7	54.5	51.9	45.5
EGFR24.M20	21:43:32.81	4.5	1872.4	82.4						74.6		-						

FILENAME	RECEIVE	BETA	S R	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	u _. 50	0.63	0.79	1.0	1.3	1.6	2,0
	TIME	(deg)	(m)															
EGFR25.M01	21:48:19.00	1.9	283.2	79.3	68.3	74.0			_					53.4			53.4	51.0
EGFR25.MØ2	21148119.02	1.6	286.3	76.1	64.8	65.8	66.2	62.7	56.9	55.0	56.7	57.5	56.0	57.9	55.5	54.8	54.4	52,2
EGFR25, MØ3	21:48:19.02	0.1	289.3	95.2	80.2	80.5	79.9	81.1	80.3	83.5	85.3	86.5	84.8	82.7	85.1	85.8	85.3	80.2
EGFR25.MØ4	21:48:19.81	0.9	510.1	80.5	70.5	65.4	67.4	68,0	62.9	63,4	64.2	70.2	67,9	64.3	62,6	65.6	68.1	61.2
EGFR25.MØ5	21:48:20.90	ð.6	812.9	96.3	78.1	80,6	76,5	70.4	73.0	73.3	80,2	85.0	87.6	88.9	89.3	89.3	83.9	76.1
EGFR25.MØ6	21:48:21.20	0.5	974.6	96.4	77.1	81,0	76.1	69.7	71.5	74.0	80.8	84.9	88.0	88.8	89,9	88.6	79.2	70,7
EGFR25,MØ7	21148122.02	0.4	1206.1	70.7	56.1	63,6	54.1	51.6	50.5	45.4	48.8	53,3	53.8	56,6	57.7	55.2	50.7	47.5
EGFR25.M08	21:48:22,91	2.3	1454.0	68.7	47.4	45.9	44.8	46.0	43.7	50.8	55,5	62.2	58.5	58.4	58.4	63.4	57.9	46.3
EGFR25, MØ9	21:48:19,68	0.3	1513.8	69.7	53.8	48.0	46.5	45.3	43.1	44.7	49.7	54.1	56.8	57.4	55.7	55.8	50.2	43.7
EGFR25.M10	21:48:19.55	0.3	1731.9	68.1	46.8	41.3	46.6	50.5	46.2	54.8	60.1	55,8	54.8	51.8	48.7	50.0	42.8	39,4
EGFR25,M11	21148119,54	0.3	1734.6	67.1	46.2	42,0	43.1	42.3	48.2	51.7	52,5	53.4	59.4	62.1	55.9	50.7	44.7	41.4
EGFR25.M12	21:48:19.55	0.0	1737.4	73.4	44.9	45.3	45.7	54.7	55. 7	61.4	66.0	64,5	68.0	60.5	58.5	55 .5	47.0	44.2
EGFR25,M13	21148119.70	1.7	314.0	91.8	72.3	71.1	73,9	75,9	81.A	81.1	82.8	82.0	83.5	82.8	79.5	80,5	79.1	74.4
EGFR25.M14	21:48:19.71	1.5	317.1	88.3	78.1	79.4	77.8	76.6	75.1	77.1	72.3	73.6	70.6	71.4	70.7	73.2	73.4	71.6
EGFR25,M15	21148119,72	0.0	320.1	86,8	76.1	74.7	73.9	75.1	76.R	76.7	77.4	73.9	69.7	68.9	69.1	71.3	72.7	67.3
EGFR25, M16	21:48:18.80	7.5	62.0	98.0	85.0	84.0	82.6	84.6	85.6	87.0	92,9	89.9	86.8	84.0	85.1	84.1	81.8	81.1
EGFR25.M17	21:48:18,80	7.5	62.2	98.1	88.9	87.9	85.5	86,9	87.6	87.9	89.5	92.1	91.6	87.7	85.7	86.1	86.1	84.9
EGFR25.M18	21:48:23,95	0.3	1499.7	67.6	53.1	49.5	51.9	55,5	53.6	54.7	54.5	57.6	56,3	52.3	51,4	46.2	45.4	41.1
EGFR25, M19	21:48:24,77	0.3	1725.3	73.1	49.8	48.4	47.3	54.5	64.1	63.6	61.2	65.0	64.4	58.8	56.0	50.8	46.7	45.2
EGFR25.M20	21:48:25,67	0.2	1979.1	67.9	46.0	51.6	53.0	54.2	63. P	58.4	56.0	57.1	53.0	46.5	46.8	43.6	42.2	37.6

FILENAME	RECEIVE	ATSB	S.R	OSPL	0.10	0.13	3,16	0,20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1,3	1.6	2.0
	TIME	(deg)	(m)															
EGFR26.MØ1	21152121,06	2.8	213.8	95.1	86.5	82.1	81.2											71 0
EGFR26.MØ2	21:52:21.08	2.4	216.8			83,0												
EGFR26.M03	21:52:21.09	0.3	219.6	100.6														-
EGFR26. MØ4	21152121.77	1.2	435.3			78.2												-
EGFR26.MØ5	21:52:22.70	0.7	730.9			59.8												
EGFR26.MØ6	21152:22.87	8.6	887.3			61.6												-
EGFR26.MØ7	21152123.59	0.5	1113.3			59.7												-
EGFR26, MØ8	21152124,35	0.4	1355.3			53.4												
EGFR26.M89	21:52:25.05	0,3	1575.6	66.1		54.4												
EGFR26.M10	21152125,82	0.3	1820.3	63.9	45.0	50.6	48.1	51.8	48.6	50.3	54.0	48.9	49.6	50.5	45.2	48.3	43.1	38,2
EGFR26.M11	21152125,83	0.3	1823.4	65.2	44,6	48.6	44.5	43.1	41.6	44.4	52.6	52.4	54.8	60.7	54.7	56,9	47.1	36,9
EGFR26.M12	21152125.84	0.0	1826.5	72.8	46,0	54.7	59.5	59.1	59.3	60.4	63.1	64.0	64.5	66.9	57.0	52,3	48.1	44.7
EGFR26,M13	21152121.84	2.4	246.8	97.6	80,4	79.0	79.3	84.2	84.7	86,6	89.7	90.1	87.5	86.2	83.2	87.8	82.2	81.7
EGFR26.M14	21152121.85	2.1	249.8	100.1	80.4	84.2	86.9	87.8	91.9	93,8	92.1	90.5	87,3	87.1	82.1	77.7	74.7	80.0
EGFR26.M15	21152121,86	0.3	252.6	102.1	79.4	87.9	90.1	88.0	90.9	95.1	94.2	92.3	89.2	89.3	90.6	89.5	90.5	88.2
EGFR26.M16	21152121.16	57.6	11.1	126.6	98.4	105.2	104.6	108.7	115.6	121.3	118.9	115.4	114.9	112.3	111.4	113,3	111.7	110.0
EGFR26.M17	21152121.16	57.6	11.1	102.5	94.9	92.9	94.4	95.0	92.9	90.2	89.1	88,8	89.9	88.0	88.5	88.1	86.9	86,3
EGFR26.M18	21152125,50	0.4	1404.4	76.8	64.3	67.6	68.6	63.3	66.3	67.6	69.1	66.4	62.7	62.3	57.0	55.4	58.1	51.8
EGFR26, M19	21:52:26.20	0.3	1624.6	73.2	62,8	62.0	61.0	60.4	60.6	64,9	63.0	63,6	63.6	62.3	53.4	52,6	51.6	47.5
EGFR26, M2Ø	21:52:26.98	0.3	1872.5	70.5	60.5	54.5	54.4	57,5	60.6	69.1	62.0	62.6	61.4	56.0	51.6	50.3	48.0	41.9

FILENAME	RECEIVE	BETA	5 २	OSPL	0.10	0.13	0.16	0.20	0.25	0,32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	5.0
	TIME	(deg)	(m)							_=								
																		-, -
EGFR27. MØ1	21155143,57	6.3	215.5									85.3						
EGFR27. M32	21:55:43,58	5.9	218.3									82,2						
EGFR27. M03	21:55:43.58	3.8	220.5	102.3														
EGFR27.M04	21:55:44.24	3.0	435.4									82.0						
EGFR27.MØ5	21155145,14	1.8	729.7									69.1						
EGFR27.M06	21:55:45.31	1.4	885.2									65.3						
EGFR27. M07	21:55:46.01	1.2	1110.4	70.5	58.6	63,9	52.7	51.4	50.2	50.8	52.7	53.8	56,9	63,1	55.0	56.2	52.4	46.4
EGFR27. MØ8	21:55:46.75	1.0	1351.4									59.4						
EGFR27. MØ9	21:55:47,43	0.8	1570.9	67.9	52.2	49.0	47.6	50.2	51.7	47.8	53,6	53.6	56,7	58.2	56.1	54.0	49.5	44.5
EGFR27. M10	21:55:48.18	0.7	1814.8	61.0	47.0	44.3	49.7	51.4	52.7	49.2	45.0	42.3	42.4	42.4	43.0	42.0	40.8	35,7
	21:55:48.19	0.7	1817.8	61.3	46.9	41.0	43.9	43.8	46.3	42.5	44.4	46.6	49.1	50.2	51.8	49.7	45.1	37.9
-	21:55:48.20	0,5	1820.8	74.8	42.3	51.7	53,7	55.1	54.A	60.6	67.2	68,2	64.4	59.7	58.1	56,3	49.6	44.0
	21:55:44,32	5,5	248.6	100.3	64.1	74.4	84.0	90.0	90.1	84.7	93,2	89,3	90.2	88.3	88.0	87.0	86,2	81.2
	21:55:44,33	5.2	251.5	100.6	80.8	84.2	85,6	92.9	91.9	92.5	94.5	90.0	82.8	79.2	86.4	90.1	89,3	82.0
-	21155144,32	3,3		105.1														
	21155143.75	57.5																
	21155:43.76			108.2	96,6	99,5	98.0	96.8	95.0	89.1	95,9	102.0	103.7	99.0	92.1	95,3	92.0	92.7
-	21155147,85		.1401.0									45.7						
	21155:48,53	•										40.5						
	21155149.28																	
EUTREI . MED	C1177144150	0,1	.00,15			- • -		•										

FILENAME	RECEIVE	BETA	sa	OSPL	0.10	0.13	0.16	0.20	0.25	0.32	0.40	0.50	0.63	0.79	1.0	1.3	1.6	2.0
	TIME	(deg)	(m)															
EGFR28, MØ1	22:22:30,00	0.1	755.6	84.0	77.6	75.0		69.3	_	_						5A 1	55 4	55 A
	22:22:30.00	0.0	758.6					68.0										
EGFR28.M23	22:22:30.00	-0.6	761.7					76.8							-		=	-
EGFR28.MØ4	22:22:30.00	2.0	974.5					59.7										
EGFR28.M05	22122148.00	-	1266.6					45.8										
EGFR28.MØ6	22:22:48.00		1438.2															
EGFR28.M07	·	-	•					45.6										-
	22:22:48.00		1661.5					46.6										
EGFR28.MØ8	22:22:38.00	-	1900.6					44,3										
EGFR28, MØ9	22:22:30.00	a.ø	2118.3	73.3	57.8	55.3	49,3	50,6	44.5	47.6	52.3	54.8	58.4	57.2	56,1	47.3	40.3	37.0
EGFR28.M10	22:22:30,00	0.0	2360.3	71.1	54.5	52.6	52.1	52.6	52.0	51.7	55.7	56,7	56.5	49.5	49.2	45.7	40.6	34.4
EGFR28.M11	22122130.00	2.0	2363,3	65,9	47.1	44.7	41.3	39.3	42.3	42.1	49.8	56.6	58.0	51.3	48,9	40.7	36.1	30,2
EGFR28.M12	22:22:30.00	-0.2	2366,4	62.1	41.8	47.5	50.5	49.7	53.1	51.3	50.5	51,9	47.5	44.5	43.7	38.4	30.7	26.8
EGFR28.M13	22122129.00	0.1	753,7	96.8	85.7	88.2	89.5	86.7	83.5	83.1	83.8	86.2	88.0	82.6	80.8	79.0	75,9	67,7
EGFR28.M14	22:22:29.00	0.0	756.7	101.6	86.5	90.1	91.7	91.9	92.7	94.4	93.3	92.7	88.2	83.5	75.7	73.1	71,3	65.5
EGFR28,M15	22:22:29.00	-0.6	759.8	102.5	86.6	90.9	92.3	92.7	93.5	95.7	94.5	93.5	89.5	85.0	76.0	77.5	76.7	68.4
EGFR28, 416	22122:29.00	Ø.0	510.0	105.7	89.6	91.6	92.7	95.1	97.5	97.1	97.2	97.5	96.0	93.8	88.0	84.8	81.9	75.1
EGFR28.M17	22:22:29.00	0.0	510.0	105.5	89.8	91.3	92.7	95.2	97.3	96.4	97.4	97.3	96.0	93.5	88.4	84.7	81.7	75.3
EGFR28. M18	22:22:35.00	a. a	1899.0					91.0										
EGFR28, M19	22:22:35,00	0.0	2116.8					89.8										
EGFR28.M2Ø	22:22:35.00	-	2362.0					87.9										
		0,0	-30-10	, C . J		U-4.	01,4	J 1 . 4	o € • 11	/ M . 3	11.0	75.5	21.0	37.0	20.0	22.2	33.n	31.7

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TABLE I.- T-38A ENGINE PARAMETERS

[Standard day]

Inlet Information: Inlet area, m ²	91 3.7 31 15 nes
Core information: Mass flow rate (station 4), kg/sec	.48 5.7 5.7 3.3
Mil. power Max. pow	wer
Jet exit diameter, m 0.31 0.785 0.33 Jet density, kg/m³ 0.785 0.33 Jet total temperature, K 958.3 1955 Jet exit velocity, m/sec 562.1 794 Nozzle pressure ratio 2.14 2. Mass flow, kg/sec 20.28 21. Ratio of specific heats 1.322 1.2	368 5.5 4.9

TABLE II.- NOMINAL AIRCRAFT OPERATING CONDITIONS

Date	Run	Altitude, m	Power sett	Time, G.m.t.		
546 0	no.	mercuacy in	Engine 1	Engine 2	Time, G.m.c.	
11/1/79	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27	9 9 10 10 10 12 12 12 12 12 18 18 18 18 18 18 18 18 18 18 18 18 18	Idle	Full burner Full burner	11 46 38 11 54 13 11 58 37 12 02 32 12 06 47 19 37 32 19 42 45 19 48 43 19 52 32 19 56 13 19 59 50 20 03 50 21 02 23 21 05 58 21 09 40 21 13 48 21 17 28 21 19 58 21 25 49 21 29 34 21 33 05 21 40 05 21 43 18 21 48 00 21 51 58 21 55 37	
	28	Static	Off	1		

TABLE III.- COORDINATES OF MICROPHONE POSITIONS

Microphone number	X, m	Y, m	Z, m
1	-243.69	53.34	0.00
2	-246.74	53.34	1.20
3	-249.78	53.34	9.14
4	-462.99	53.34	1.20
5	-755.45	53.34	1.20
6	-926.01	79.25	1.20
7	-1149.61	79.25	1.20
8	-1388.97	79.25	1.20
9	-1606.81	79.25	1.20
10	-1848.92	79.25	.00
11	-1851.96	79.25	1.20
12	-1855.01	79.25	9.14
13	-243.69	.00	.00
14	-246.74	.00	1.20
15	-249.78	.00	9.14
16	.00	.30	1.20
17	.00	.00	1.20
18	-1388.97	.00	1.20
19	-1606.81	.00	1.20
20	-1851.96	.00	1.20

TABLE IV.- SAMPLE WEATHER DATA FOR RUN 27

Height and location of weather station	Wind speed, m/sec	Wind direction, deg	Temperature, OC	Atmospheric pressure, kPa	Humidity, percent	Dew point,
1.2 m, van 1 1.2 m, van 5 10 m, van 3 10 m, N-159 10 m, C-15 3 m, triangle area 6 m, triangle area 9 m, triangle area 12 m, triangle area	1.8 1.4 1.4 1.8 2.7 2.2 2.4 2.5 2.4	300 270 359 285 285 296 288 275 275 295	13.3 12.2 14.0 15.0	101.8 101.9	39.0	-18

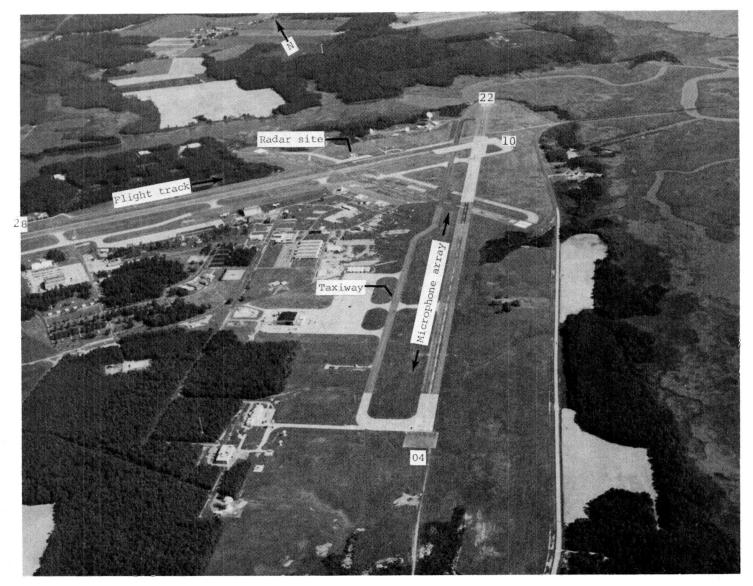
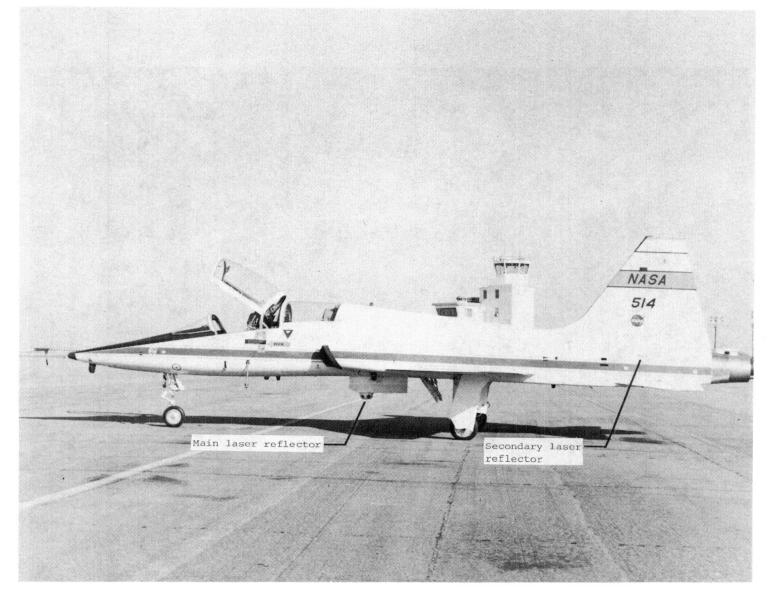
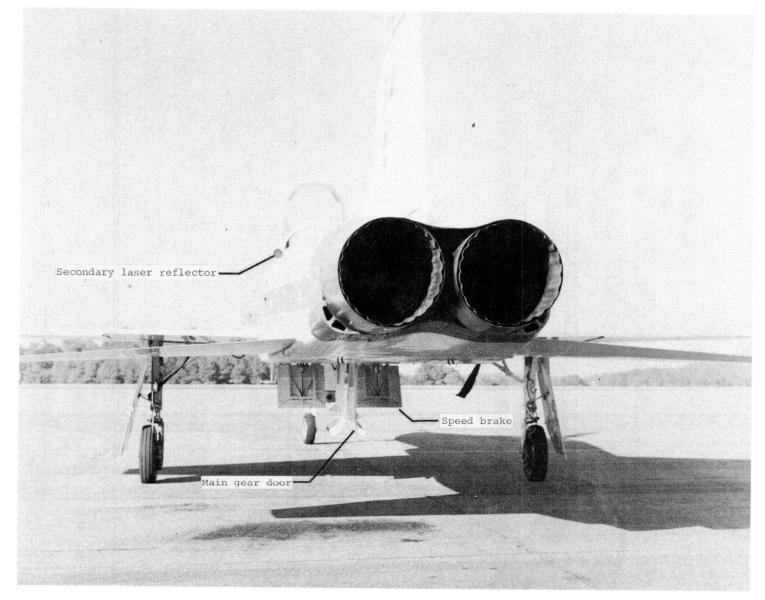


Figure 1.- Experimental site.



(a) Side view.

Figure 2.- Noise source.



(b) Rear view.

Figure 2.- Concluded.

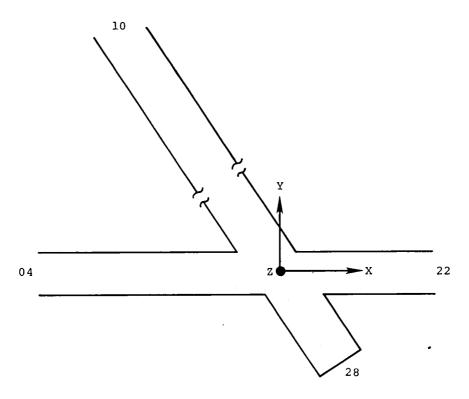


Figure 3.- Data reduction coordinates.

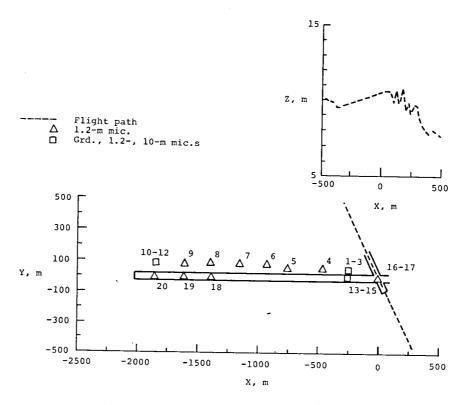


Figure 4.- Flight track for run 26.

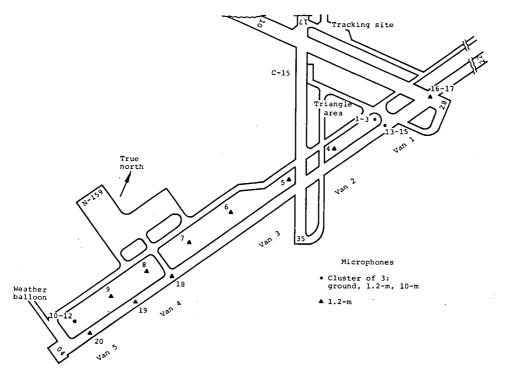


Figure 5.- Diagram of experimental site.

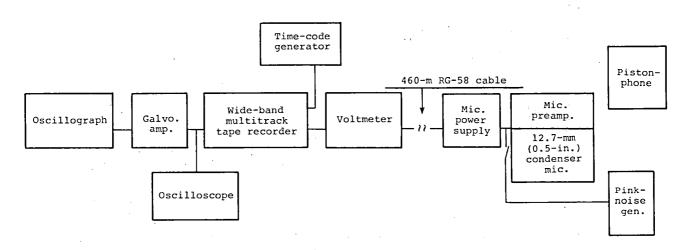
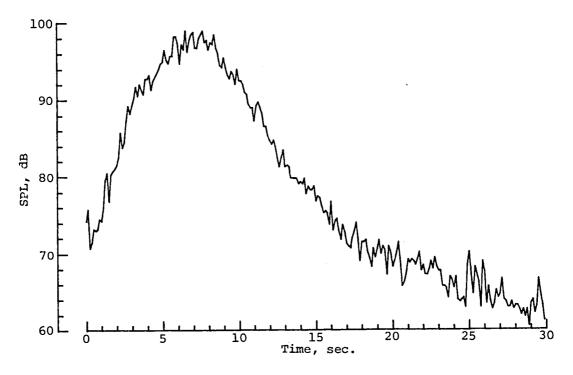


Figure 6.- Block diagram of acoustic instrumentation.



(a) Microphone 2.

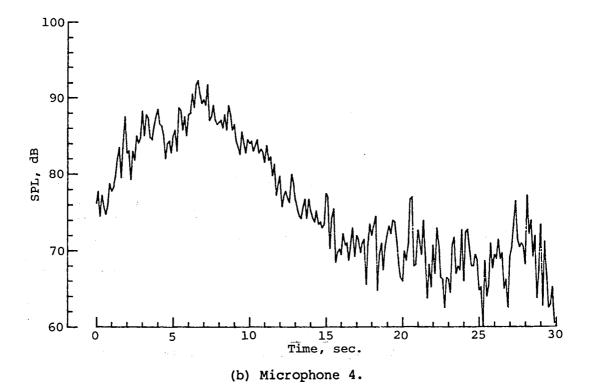
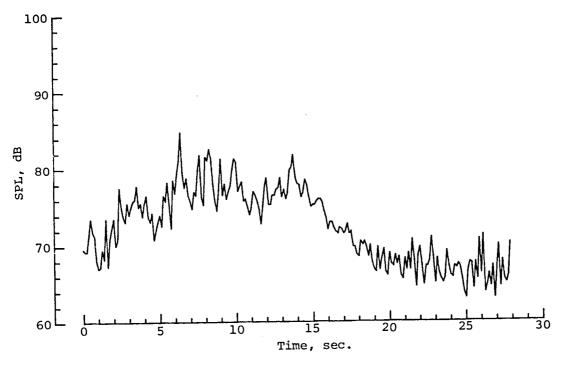
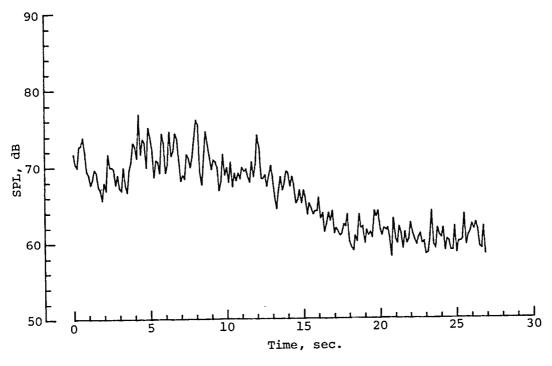


Figure 7.- Time histories for run 27.



(c) Microphone 6.



(d) Microphone 8.

Figure 7.- Concluded.

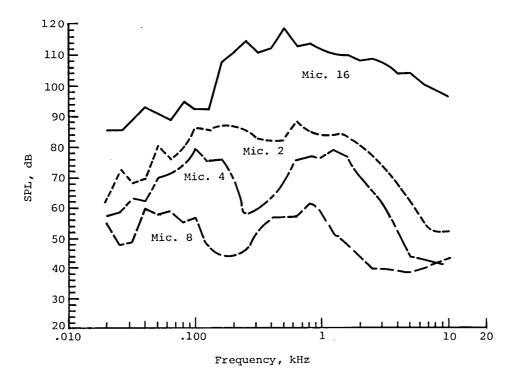


Figure 8.- Maximum overall spectra for run 27.

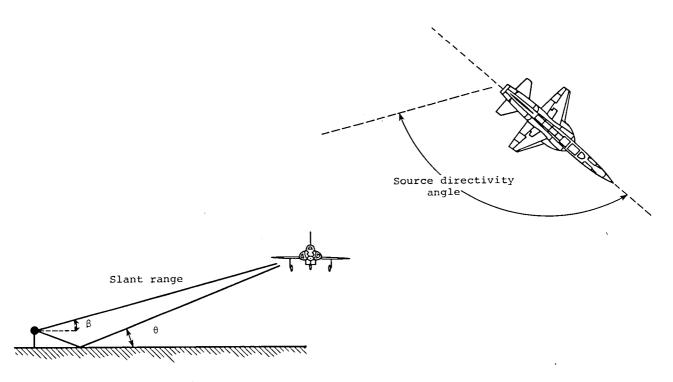


Figure 9.- Source-microphone geometry.

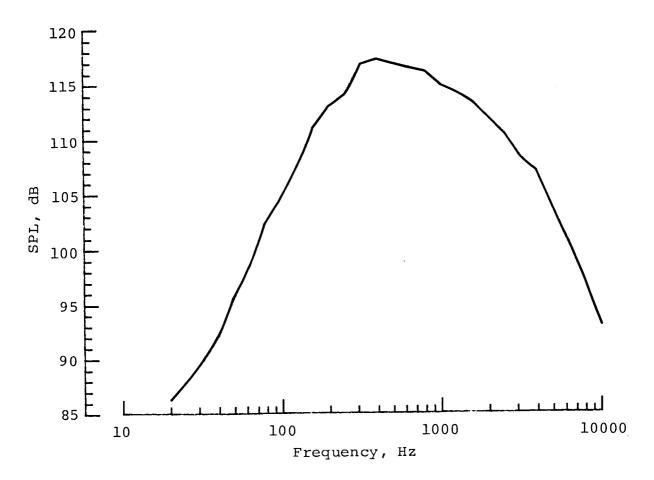
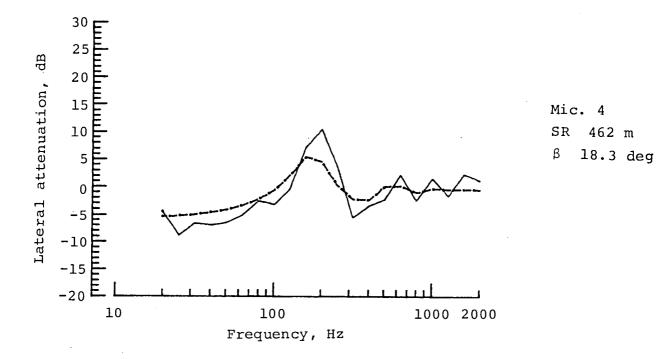


Figure 10.- Reference spectrum for near/far comparison method.



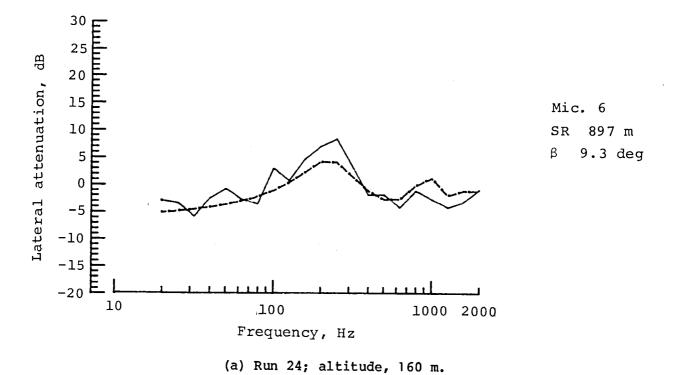
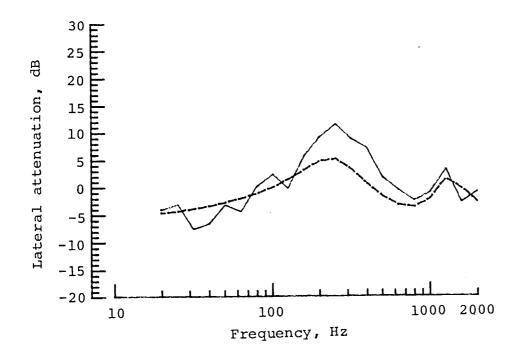
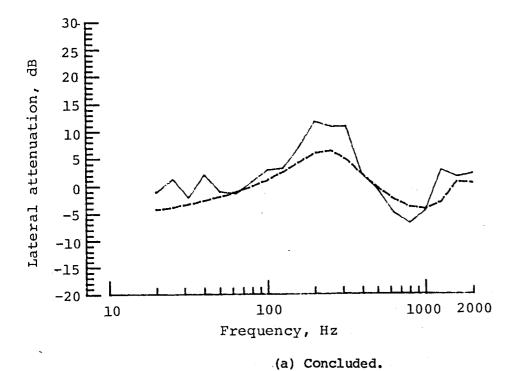


Figure 11.- Near/far results. Solid curve, measured results; dashed curve, predicted results.

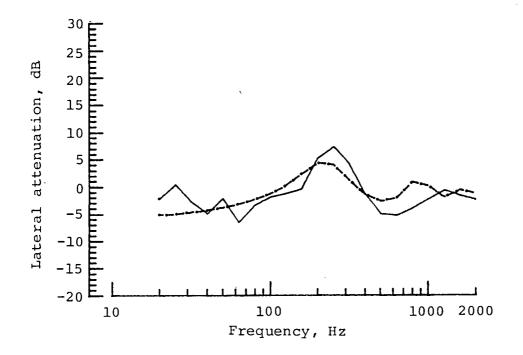


Mic. 8 SR 1358 m β 6.1 deg

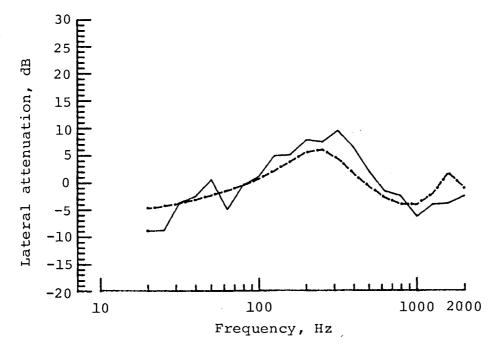


Mic. 11 SR 1823 m β 4.6 deg

Figure 11.- Continued.



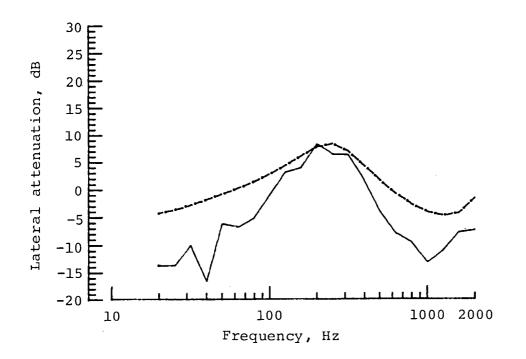
Mic. 4 SR 433 m β 10.0 deg



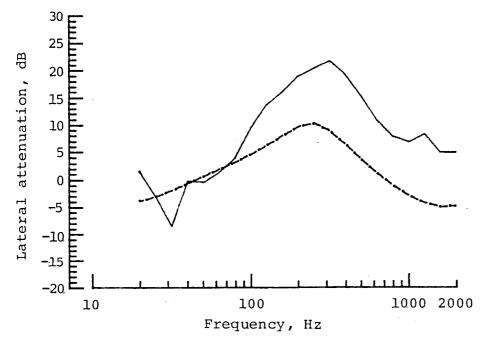
Mic. 6 SR 885 m β 4.9 deg

(b) Run 21; altitude, 80 m.

Figure 11.- Continued.



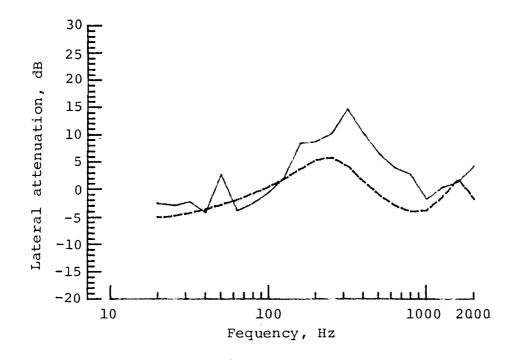
Mic. 8 SR 1355 m β 3.2 deg



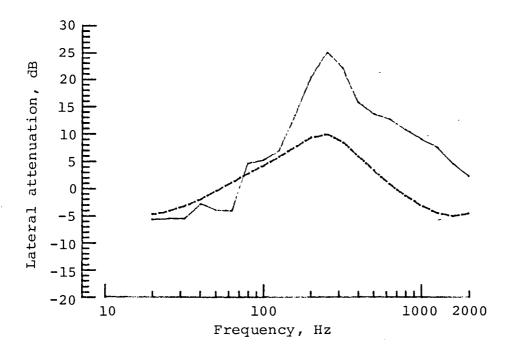
Mic. 11 SR 1826 m β 2.4 deg

(b) Concluded.

Figure 11.- Continued.



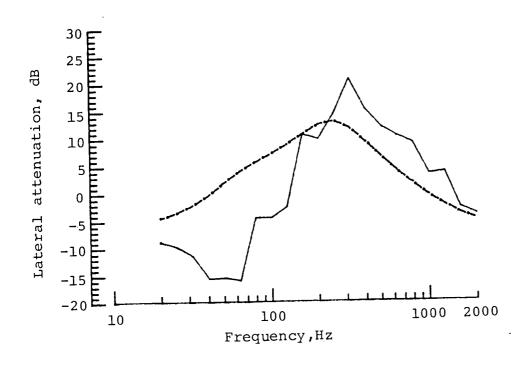
Mic. 4 SR 433 m β 5.0 deg



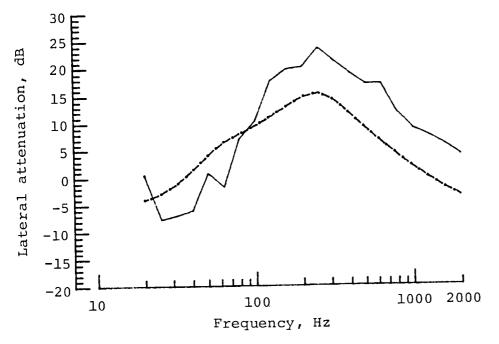
Mic. 6 SR 884 m β 2.5 deg

(c) Run 17; altitude, 40 m.

Figure 11.- Continued.



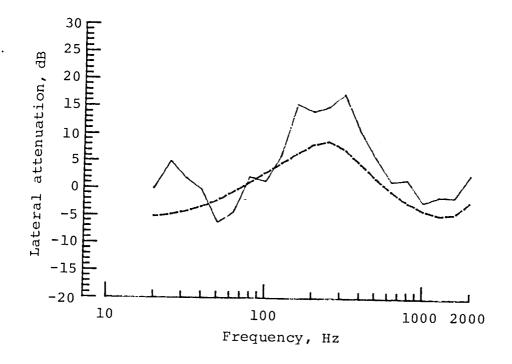
Mic. 8 SR 1351 m β 1.6 deg



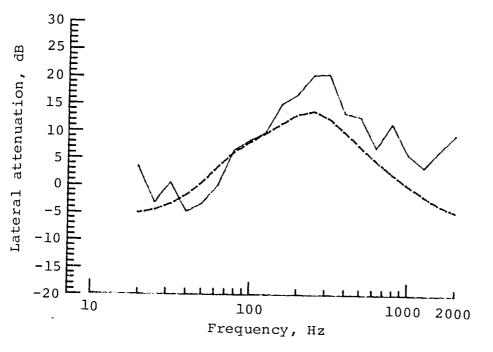
Mic. 11 SR 1819 m β 1.2 deg

(c) Concluded.

Figure 11.- Continued.



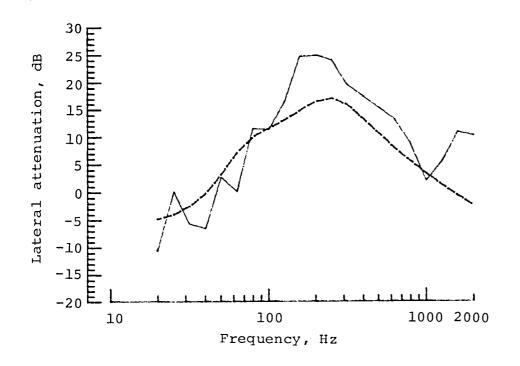
Mic. 4 SR 435 m β 3.0 deg



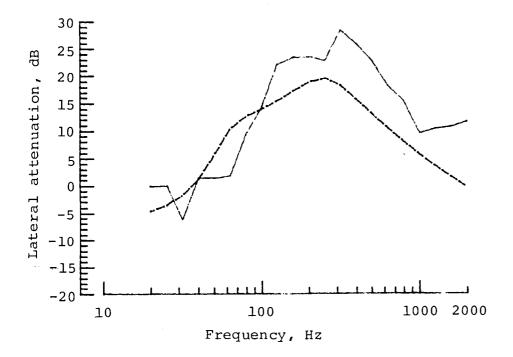
Mic. 6 SR 885 m β 1.4 deg

(d) Run 27; altitude, 20 m.

Figure 11.- Continued.



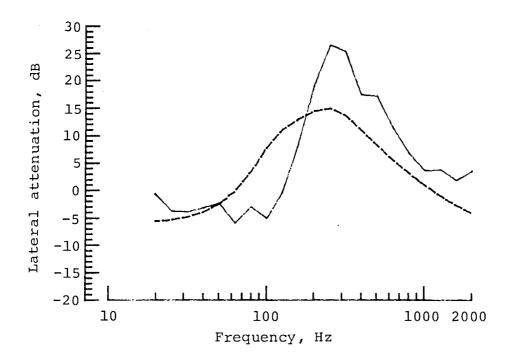
Mic. 8 SR 1351 m β 1.0 deg



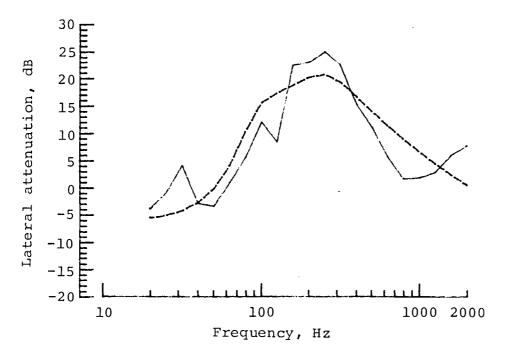
Mic. 11 SR 1818 m β 0.7 deg

(d) Concluded.

Figure 11.- Continued.

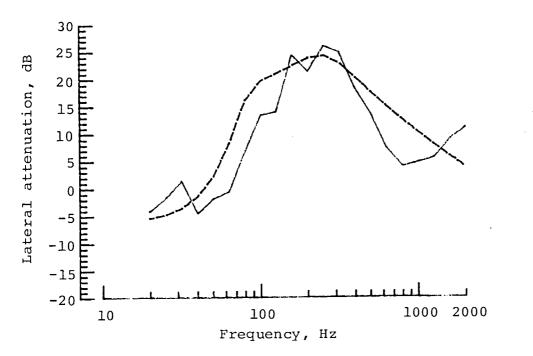


Mic. 4 SR 435 m β 1.2 deg

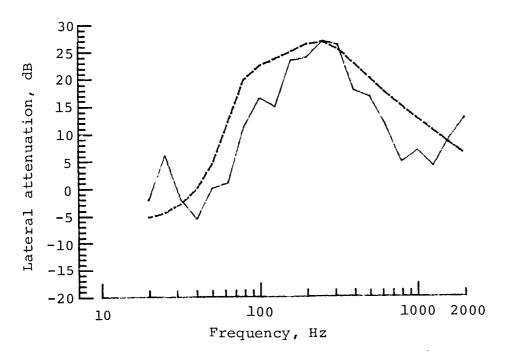


Mic. 6 SR 887 m β 0.6 deg

(e) Run 26; altitude, 10 m.
Figure 11.- Continued.



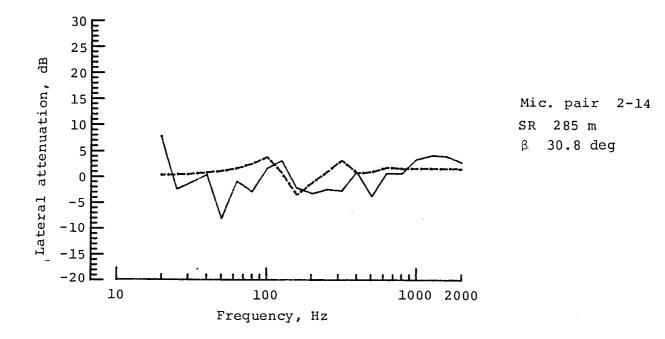
Mic. 8 SR 1355 m β 1.0 deg



Mic. 11 SR 1823 m β 0.3 deg

(e) Concluded.

Figure 11.- Concluded.



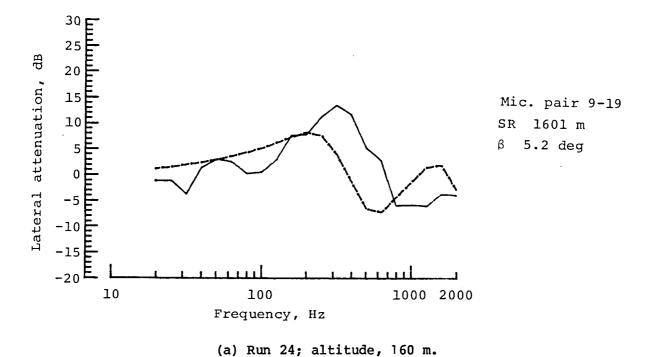
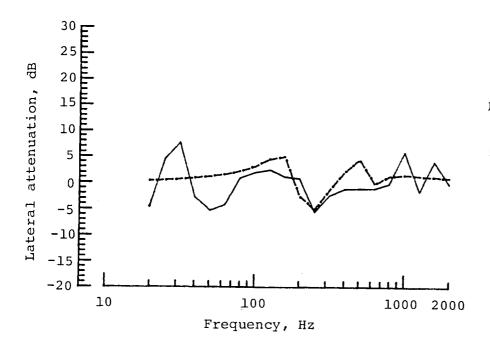
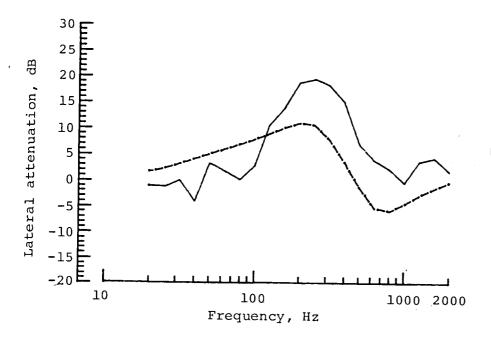


Figure 12.- Direct results. Solid curve, measured results; dashed curve, predicted results.

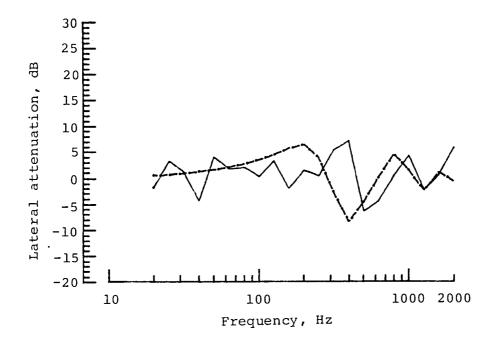


Mic. pair 2-14 SR 237 m β 18.7 deg

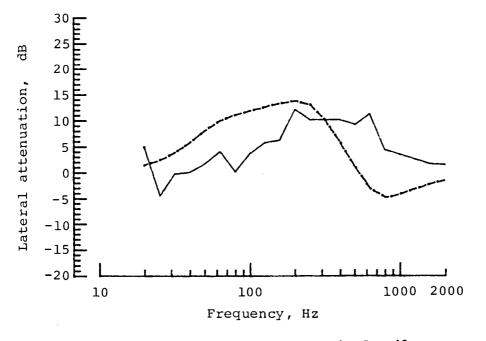


Mic. pair 9-19 SR 1601 m β 2.7 deg'

(b) Run 21; altitude, 80 m.
Figure 12.- Continued.



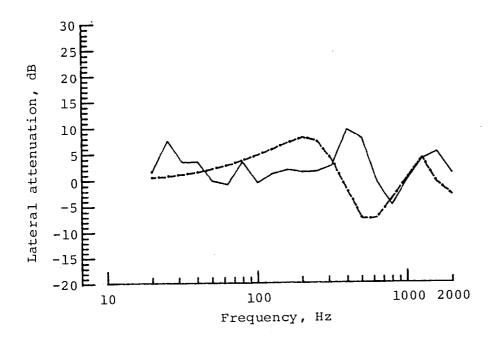
Mic. pair 2-14 SR 233 m β 9.4 deg



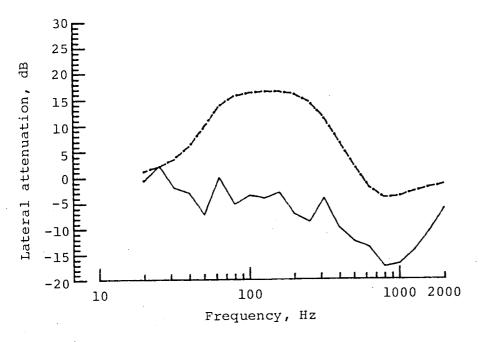
Mic. pair 9-19 SR 1596 m β 1.4 deg

(c) Run 17; altitude, 40 m.

Figure 12.- Continued.

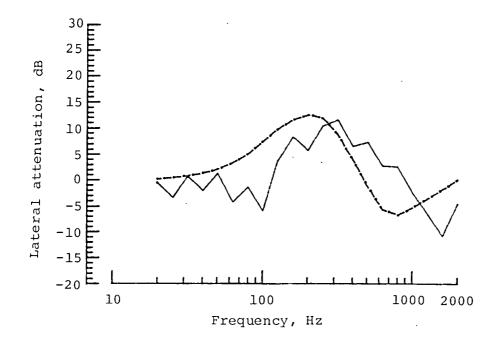


Mic. pair 2-14 SR 235 m $$\beta$$ 5.5 deg

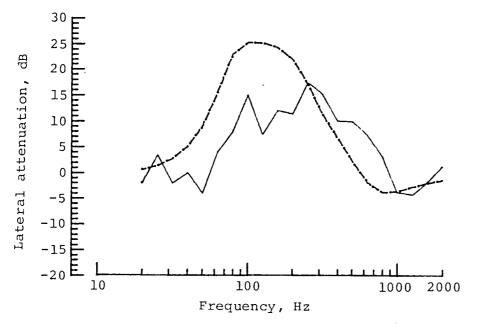


Mic. pair 9-19 SR 1596 m β 0.8 deg

(d) Run 27; altitude, 20 m.
Figure 12.- Continued.

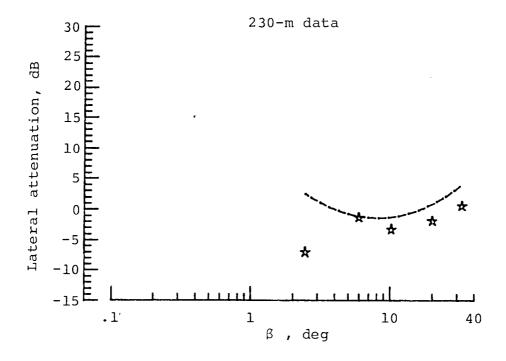


Mic. pair 2-14 SR 233 m β 2.3 deg



Mic. pair 9-19 SR 1600 m β 0.3 deg

(e) Run 26; altitude, 10 m.
Figure 12.- Concluded.



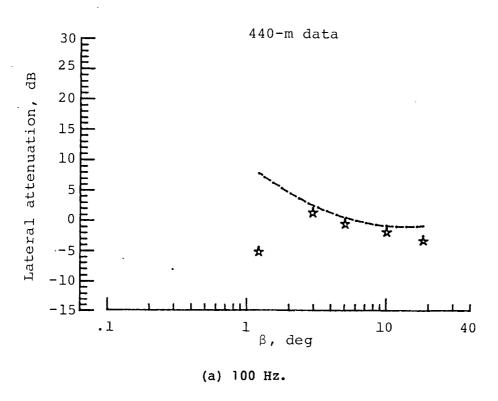
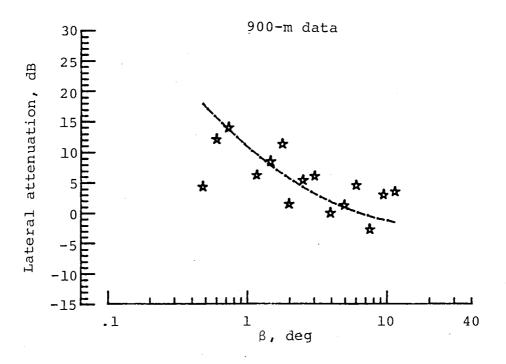


Figure 13.- Near/far results. Symbols, measured results; curves, predicted results.



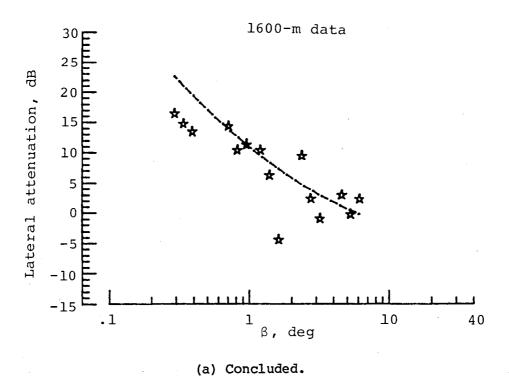
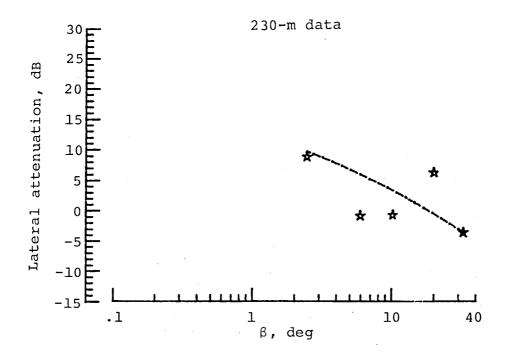


Figure 13.- Continued.



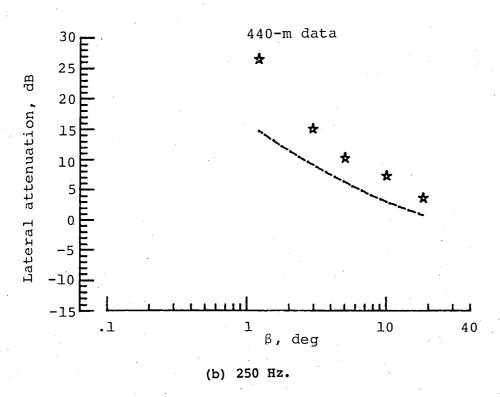
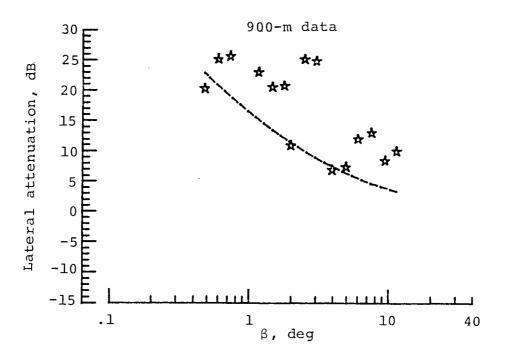


Figure 13.- Continued.



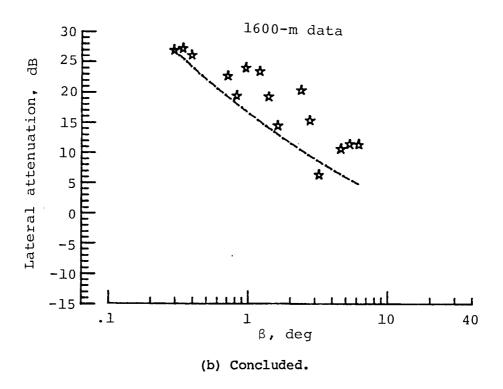
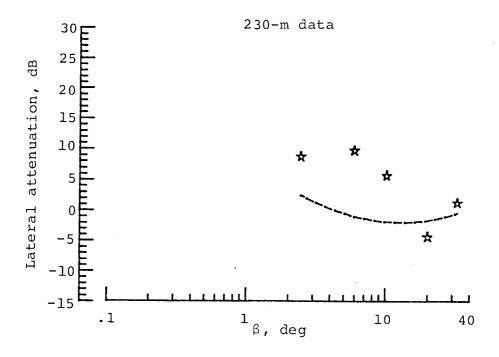


Figure 13.- Continued.



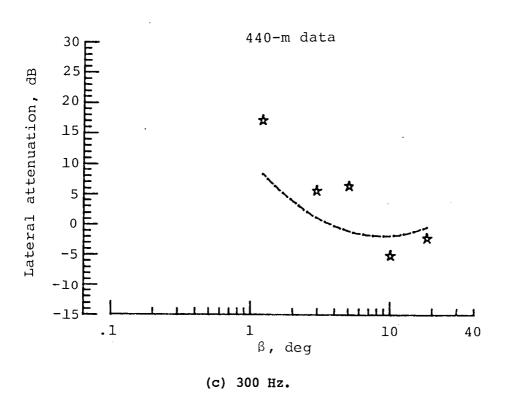
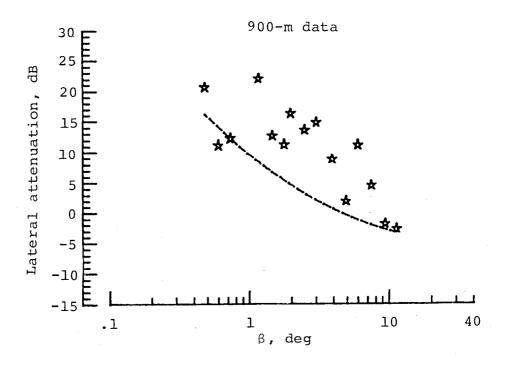


Figure 13.- Continued.



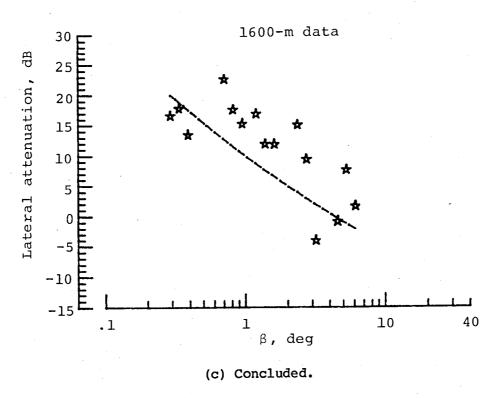
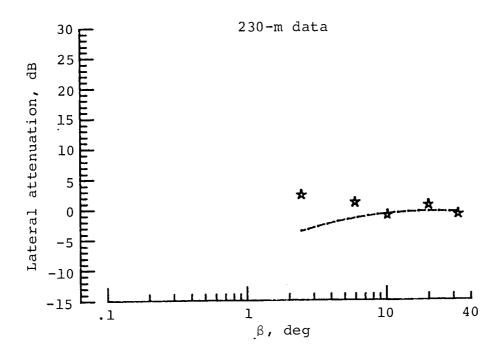


Figure 13.- Continued.



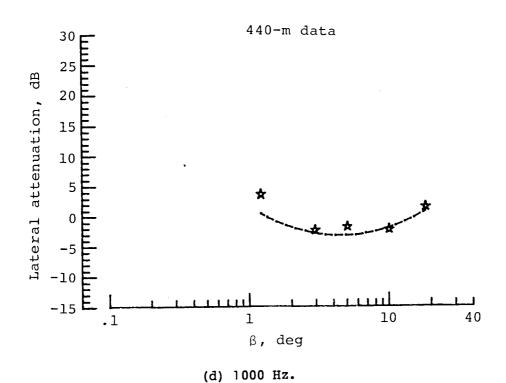
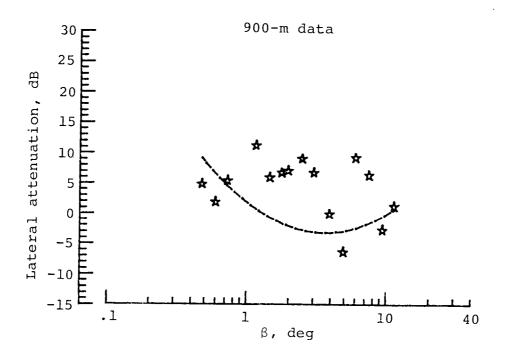


Figure 13.- Continued.



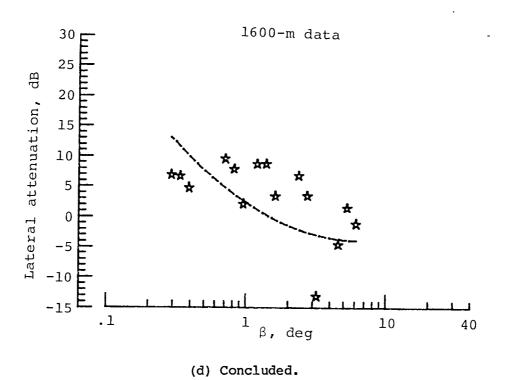
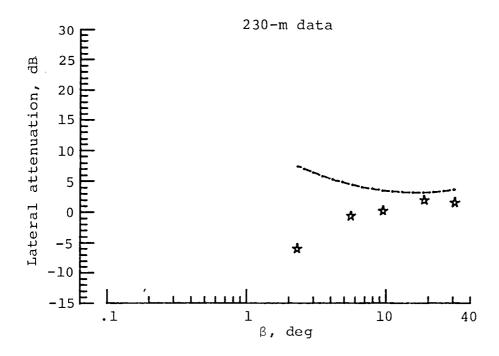


Figure 13.- Concluded.



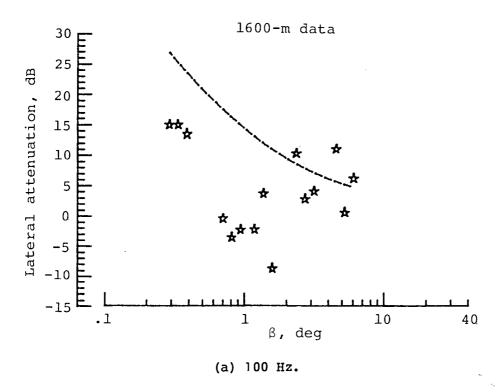
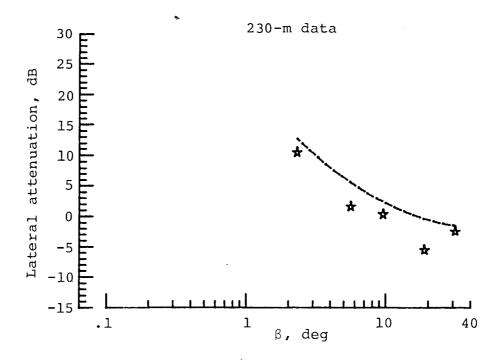


Figure 14.- Direct results. Symbols, measured results; curves, predicted results.



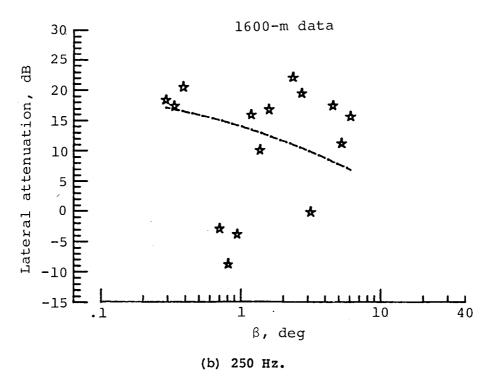
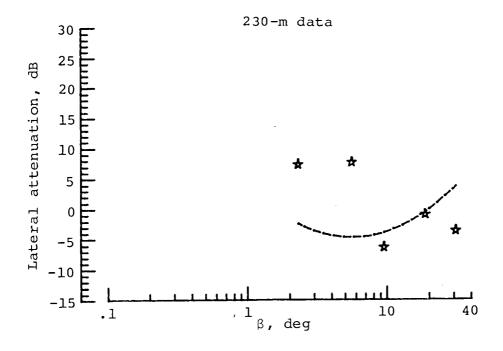


Figure 14.- Continued.



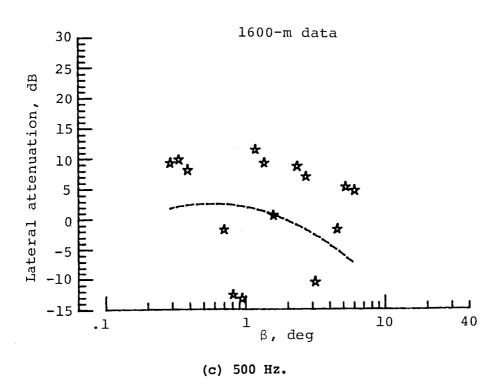
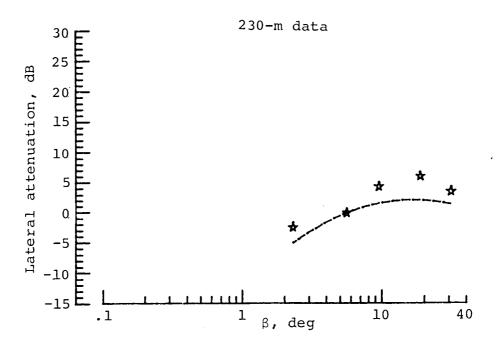


Figure 14.- Continued.



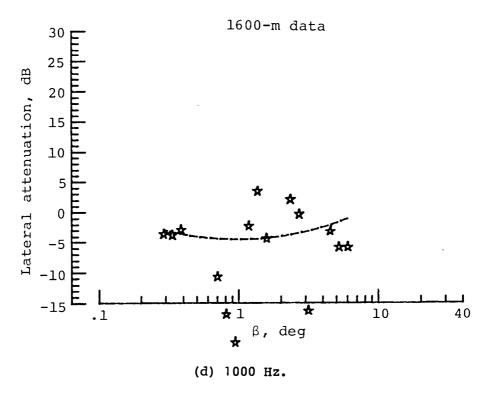


Figure 14.- Concluded.

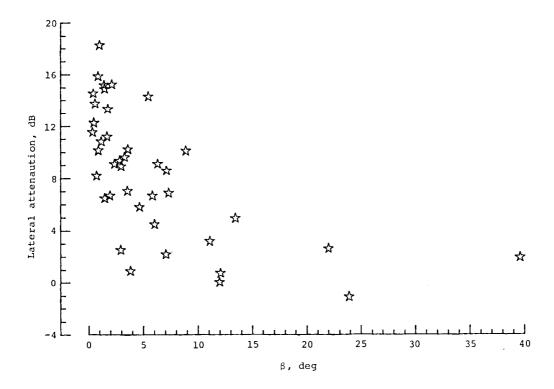


Figure 15.- Near/far results in EPNL units.

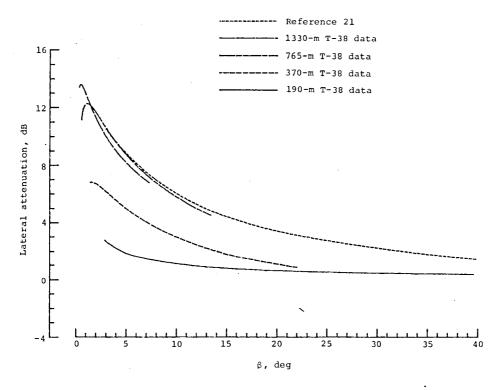


Figure 16.- Near/far results in EPNL units. Dependence on slant range.

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A flight experiment was conducted to investigate air-to-ground propagation of sound at grazing angles of incidence. A turbojet-powered airplane was flown at altitudes ranging from 10 to 160 m over a 20-microphone array positioned over grass and concrete. Acoustic, tracking, and weather data are presented in the appendices. The dependence of ground effects on frequency, incidence angle, and slant range has been determined using two analysis methods. In one method, a microphone close to the flight path is compared to down-range microphones. In the other method, comparisons are made between two microphones which were equidistant from the flight path but positioned over the two surfaces. In both methods, source directivity angle was the criterion by which portions of the microphone signals were compared. The ground effects were largest in the frequency range of 200 to 400 Hz and were found to be dependent on incidence angle and slant range. Ground effects measured for angles of incidence greater than 10° to 15° were near zero. Measured attenuation increased with increasing slant range for slant ranges less than 750 m. Theoretical predictions were found to be in good agreement with the major details of the measured results.				
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